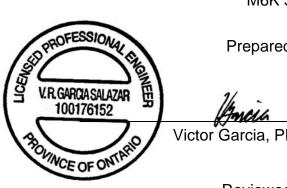


Howe Gastmeier Chapnik Limited 2000 Argentia Road, Plaza One, Suite 203 Mississauga, Ontario, Canada L5N 1P7 t: 905.826.4044

Noise Feasibility Study Proposed Stacked Townhouse Development 1575 Hurontario Street Mississauga, Ontario

Prepared for:

Dream Maker Inc. Attn: Isaac Olowolafe 59 East Liberty Street Toronto, Ontario M6K 3R1



Prepared by

Victor Garcia, PEng

Reviewed by

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August 16, 2017

Project No: 01700181





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Figure 1: Aerial Photo of SiteFigure 2: Proposed Site PlanFigure 3: Proposed Site Plan Showing Ventilation Requirements

Appendix A: Supporting Drawings

Appendix B: Road Traffic Information

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1 Introduction & Summary

HGC Engineering was retained by Dream Maker Inc. to conduct a noise feasibility study for a proposed stacked townhouse development to be located at 1575 Hurontario Street, in Mississauga, Ontario. The proposed development will include two 3 ½ -storey stacked back to back townhouses townhouse blocks. The study is required by the Municipality as part of the planning and approvals process.

The primary sources of noise impacting the site were determined to be road traffic on Hurontario Street and the Queen Elizabeth Way (QEW). Relevant road traffic data was obtained from the Ministry of Transportation (MTO) and the City of Mississauga, and was used to predict future traffic sound levels at the locations of the proposed residential dwelling facades. The predicted sound levels were compared to the guidelines of the Ministry of Environment and Climate Change (MOECC) and the Municipality to develop noise control recommendations.

The sound level predictions indicate that the future road traffic sound levels will exceed MOECC guidelines at all townhouse blocks. Central air conditioning systems are required for all the townhouse units. Upgraded building and glazing constructions are required for all the dwellings. Associated acoustical requirements are specified in this report. Warning clauses are recommended to inform future residents of the road traffic noise impacts and to address sound level excesses.







2 Site Description & Noise Sources

The proposed residential development is located at 1575 Hurontario Street in the City of Mississauga, Ontario. Figure 1 shows a key plan illustrating the location of the subject site. A site plan prepared by Kirkor Architects + Planners dated May 8, 2017 is shown in Figure 2. The proposed development will consist of two blocks of 3 ¹/₂ -storey stacked back to back townhouses and associated roadways. Appendix A includes the preliminary sections and elevations.

A site visit was made by HGC Engineering personnel in March 2017 to make observations of the acoustic environment, and to identify the significant noise sources in the vicinity. The acoustical environment surrounding the site is urban in nature, with existing residences to the east, west and south. Immediately to the north of the site is the New Port Credit Centre. Futher to the north is the Queen Elizabeth Senior Public School and Ontario Provincial Police facility.

Road traffic on Hurontario Street and the QEW were confirmed to be the primary sources of sound impacting the site. The QEW includes three lanes and a merging lane in each direction, while Hurontario Street currently consists of six lanes in each direction. There were no other significant sources of stationary noise noted within 500 m of the subject site.

There is a proposed future Light Rail Transit (LRT) system along the centre of Hurontario Street. Information regarding the Hurontario-Main LRT line was obtained from the report prepared for SNC-Lavalin Inc. in support of Transit Project Assessment Process (TPAP) by J.E. Coulter Associates Ltd. The report states that the LRT line will run along the Hurontario and Main Street corridor, beginning at the Port Credit GO Station and ending at the Brampton GO Transit Station. The findings of the report prepared by J.E. Coulter Associates Limited for the future Hurontario-Main Street LRT indicate that there will be no noticeable change in the sound levels along most parts of the corridor and that the contribution of the LRT in relation to the overall sound level from cars and buses is negligible. Supporting documents from the report are attached in Appendix A.







3 Noise Level Criteria

3.1 Road Traffic Noise

Guidelines for acceptable levels of road traffic noise impacting residential developments are given in the MOECC publication NPC-300, "Environmental Noise Guideline Stationary and Transportation Sources – Approval and Planning", release date October 21, 2013 and are listed in Table 1 below. The values in Table I are energy equivalent (average) sound levels [L_{EQ}] in units of A-weighted decibels [dBA].

Space	Daytime L _{EQ} (16 hour) Road	Nighttime L _{EQ} (8 hour) Road			
Outdoor Living Areas	55 dBA				
Inside Living/Dining Rooms	45 dBA	45 dBA			
Inside Bedrooms	45 dBA	40 dBA			

Table I: MOECC Road Traffic Noise Criteria [dBA]

Daytime refers to the period between 07:00 and 23:00, while nighttime refers to the period between 23:00 and 07:00. The term "Outdoor Living Area" (OLA) is used in reference to an outdoor patio, a backyard, a terrace or other area where passive recreation is expected to occur. Balconies that are less than 4 m in depth are not considered to be outdoor living areas under MOECC guidelines.

The MOECC guidelines allow the daytime sound levels in OLA to be exceeded by up to 5 dBA, without mitigation, if warning clauses are placed in the purchase and rental agreements to the property. Where OLA sound levels exceed 60 dBA, physical mitigation is recommended to reduce the OLA sound level to below 60 dBA and as close to 55 dBA as technically, economically and administratively feasible.

A central air conditioning system is required for dwellings where nighttime sound levels outside bedroom or living/dining room windows exceed 60 dBA or daytime sound levels outside bedroom or living/dining room windows exceed 65 dBA. Forced-air ventilation systems with ducts sized to accommodate the future installation of air conditioning by the occupant is required when nighttime sound levels at bedroom or living/dining room windows are in the range of 51 to 60 dBA or when daytime sound levels at bedroom or living/dining room windows are in the range of 56 to 65 dBA.







Building components such as walls, windows and doors must be designed to achieve indoor sound level criteria when the plane of window nighttime sound level is greater than 60 dBA or the daytime sound level is greater than 65 dBA due to road traffic noise.

Warning clauses to notify future residents of possible noise excesses are also required when nighttime sound levels exceed 50 dBA at the plane of the bedroom or living/dining room window and daytime sound levels exceed 55 dBA in the outdoor living area and at the plane of the bedroom or living/dining room window due to road traffic.

4 Traffic Noise Assessment

4.1 Road Traffic Data

Road traffic information for Hurontario Street was obtained from the City of Mississauga, in the form of ultimate Average Annual Daily Traffic (AADT) values, and is provided in Appendix B. An ultimate AADT of 48 000 vehicles per day, along with a speed limit of 50 km/h, was applied to Hurontario Street. A commercial vehicle percentage of 10% was used in the analysis and was further split into 5.5% and 4.5% for medium and heavy trucks, respectively.

Road traffic data for the QEW was obtained from the Ministry of Transportation (MTO), in the form of Summer Average Daily Traffic (SADT) values for the year 2013, and is provided in Appendix B. A SADT of 187 000 vehicles per day, along with a posted speed limit of 100 km/h, was applied to the QEW. The data was projected to the year 2027 using a 2.5 % growth rate. A commercial percentage of 12.0% was further split into 3.0% medium trucks and 9.0% heavy trucks, and was used in the analysis as per MTO procedures. A day/night split of 88%/12% for the QEW was obtained from HGC Engineering project files for other projects in the area and was applied to the roadway. Table II summarizes the traffic volume data used in this study.







Road Name	Cars	Medium Trucks	Heavy Trucks	Total		
	Daytime	38 880	2 376	1 944	43 200	
Hurontario Street	Nighttime	4 320	264	216	4 800	
(Ultimate)	Total	43 200	2 640	2 160	48 000	
OFW	Daytime	204 616	6 976	20 926	232 518	
QEW (Projected to 2027)	Nighttime	27 902	952	2 854	31 708	
(Frojecieu 10 2027)	Total	232 518	7 928	23 780	264 226	

Table II: Projected and Ultimate Road Traffic Data

4.2 Road Traffic Noise Predictions

To assess the levels of road traffic noise which will impact the site in the future, predictions were made using STAMSON version 5.04, a computer algorithm developed by the MOECC. Sample STAMSON output is included in Appendix C.

Prediction locations were chosen around the residential site to obtain a good representation of the future sound levels at the dwellings with exposure to the QEW and Hurontario Street. Sound levels were predicted at the plane of the top storey bedroom and/or living/dining room windows during daytime and nighttime hours to investigate ventilation requirements. The results of these predictions are summarized in Table III.

The distance setback of the buildings indicated on the site plan were used in the analysis, along with an aerial photo to determine the distance to the major roadways. In accordance with MOECC guidelines, Hurontario Street and the QEW were divided into two segments. The acoustic requirements may be subject to modifications if the site plan is changed significantly.





Prediction Location	Description	Daytime - at Façade L _{EQ(16)}	Nighttime - at Façade L _{EQ(8)}		
А	Building A, west façade	72	66		
В	Building A, north façade	70	64		
С	Building A, south façade	68	61		
D	Building B, north façade	67	61		
E	Building B, south façade	63	56		
F	Building B, north façade	67	61		

Table III: Predicted Road Traffic Sound Levels [dBA], Without Mitigation

5 Traffic Noise Recommendations

The predictions indicate that the future traffic sound levels will exceed MOECC guidelines at all the townhouse units within the development with exposure to Hurontario Street and the QEW. The following discussion outlines recommendations for acoustic barriers, ventilation requirements, upgraded building façade constructions, and warning clauses to achieve the noise criteria stated in Table I.

5.1 Outdoor Living Areas

The dwelling units may have balconies that are less than 4 m in depth. The section drawing provided in Appendix A indicates the rooftop amenity areas are less than 4 m in depth. These balconies are not considered to be outdoor living areas under MOECC guidelines, and therefore are exempt from traffic noise assessment.

There are no common outdoor amenity areas identified on the site plan.

5.2 Indoor Living Areas & Ventilation Requirements

The predicted daytime and nighttime sound levels outside the top storey bedroom and/or living/dining room of all future dwellings with exposure to Hurontario Street and the QEW will be greater than 65 dBA and 60 dBA respectively. To address these excesses, the MOECC guidelines recommend that the residential blocks be equipped with central air conditioning systems, so that the windows can be closed.







Figure 3 shows the ventilation requirements for the development. Window or through-the-wall air conditioning units are not recommended for any commercial or residential units because of the noise they produce and because the units penetrate through the exterior wall which degrades the overall noise insulating properties of the envelope. The location, installation and sound ratings of the outdoor air conditioning devices should minimize noise impacts and comply with criteria of MOECC publication NPC-300, as applicable. The guidelines also recommend warning clauses for all of the dwellings.

5.3 Building Façade Constructions

Predicted sound levels at the building façades were used to determine sound insulation requirements of the building envelope. The required acoustic insulation of the wall and window components was determined using methods developed by the National Research Council (NRC).

Exterior Wall Constructions

The exterior walls of the proposed stacked townhouses include brick on the upper two floors and stone on the bottom floors. The proposed building constructions will provide sufficient acoustical insulation.

Exterior Doors

There may be swing doors and some glazed sliding patio doors for entry onto the balconies from living/dining rooms and some bedrooms. The glazing areas on the doors have been counted as part of the total window glazing area. If exterior swing doors are to be used, they shall be insulated metal doors equipped with head, jamb and threshold weather seals.

Acoustical Requirements for Glazing

The preliminary floor plans and building elevations prepared by Kirkor Architects + Planners dated May 8, 2017 were used in the analysis (Appendix A). Based on the floor plans and building elevations, the calculated window to floor area ratios for both buildings are up to 24% for living/dining rooms and 27% for bedrooms. Based on the window to floor area ratios and proposed building façade constructions, any double glazed window construction meeting the minimum





VIBRATION

requirements of the Ontario Building Code (OBC) will provide adequate sound insulation for the buildings.

5.4 Warning Clauses

The MOECC guidelines recommend that warning clauses be included in the property and tenancy agreements and offers of purchase and sale for all townhouse blocks with anticipated traffic sound level excesses. The following noise warning clauses are required for specific units as indicated in Table IV.

Suggested wording for the blocks with sound levels exceeding the MOECC criteria is given below:

Type A:

Purchasers/tenants are advised that despite the inclusion of noise control features in the development and within the building units, sound levels due to increasing road traffic may on occasion interfere with some activities of the dwelling occupants as the sound levels exceed the sound level limits of the Municipality and the Ministry of the Environment and Climate Change.

Suitable wording for future buildings requiring central air conditioning systems is given below.

Type B:

This unit has been supplied with a central air conditioning system which allows windows and exterior doors to remain closed, thereby ensuring that the indoor sound levels are within the noise criteria of the Municipality and the Ministry of the Environment and Climate Change.

These sample clauses are provided by the MOECC as examples and can be modified by the Municipality as required.

6 Impact of the Development on the Environment

It is expected that any increase in local traffic associated with the development will not be substantial enough to affect noise levels significantly.

MOECC Publication NPC-300 stipulate sound level limits for new stationary (non-traffic) sources of noise. The sound level limit for a stationary source which operates in a Class 1 urban environment is related to the minimum one-hour L_{EQ} ambient (background) sound level, at any potentially impacted







residential point of reception. HGC Engineering has not performed monitoring of the background sound levels in the area during all daytime and nighttime hours, but experience indicates that, for a typical urban environment, a minimum daytime sound level of 50 dBA and a minimum nighttime sound level of 45 dBA can be assumed during the quietest hours. These criteria apply to equipment such as rooftop air-conditioners, cooling towers, exhaust fans, standby generators, etc.

Provided air-conditioning equipment recommended in item 5.2 is selected and placed appropriately so as not to impact the existing residential and proposed residential dwellings, noise impacts are not expected. An acoustical consultant should review the design of the mechanical building systems and the equipment selections when they have been determined, to help ensure that the noise levels emitted by the development to the environment are likely to meet the bylaw requirements.

7 Impact of the Development on Itself

The impact of the development on itself can be categorized into noise intrusions transmitted between adjacent spaces, and noise generated by mechanical systems or other equipment within the building.

Section 9.11.1 of the Ontario Building Code (OBC) specifies the minimum required sound insulation characteristics for demising partitions, in terms of Sound Transmission Class (STC) values. In order to maintain adequate acoustical privacy between separate suites in a multi-tenant building, inter-suite walls should meet or exceed STC-50. Walls separating a suite from a noisy space such as a refuse chute, or elevator shaft, should meet or exceed STC-55. Tables 1 and 2 in Section SB-3 of the Supplementary Guideline to the OBC provide a comprehensive list of constructions that will meet the above requirements. It is recommended that partitions be selected 3 to 4 points above tables so that performance in the field meets these minimum specifications.

Tarion's Builder Bulletin B19R requires the internal design of condominium projects to integrate suitable acoustic features to insulate the suites from noise from each other and amenities in accordance with the OBC, and limit the potential intrusions of mechanical and electrical services of the buildings on its residents. If B19R certification is needed, an acoustical consultant is required to review the mechanical and electrical drawings and details of demising constructions and mechanical/electrical equipment, when available, to help ensure that the noise impact of the development on itself is maintained within acceptable levels.





VIBRATION

8 Summary & Recommendations

The following list and Table IV summarize the recommendations made in this report. The reader is referred to the Figure 3, as well as previous sections of the report where these recommendations are applied and discussed in more detail.

- Central air conditioning is required for the proposed stacked townhouse blocks. The location, installation and sound rating of the outdoor condensing units must be compliant with MOECC Guideline NPC-300, as applicable.
- 2. With the proposed building exterior constructions, any double glazed window construction and meeting the minimum requirements of the OBC will provide adequate sound insulation for the buildings.
- 3. Noise warning clauses to inform the occupants of the sound level excesses should be placed in the property and tenancy agreements and offers of purchase and sale.
- 4. Tarion Builder's Bulletin B19R requires that the internal design of condominium projects integrates suitable acoustic features to insulate the suites from noise from each other and amenities in accordance with the OBC, and limit the potential intrusions of mechanical and electrical services of the buildings on its residents. If B19R certification is needed, an acoustical consultant is required to review the mechanical and electrical drawings and details of demising constructions and mechanical/electrical equipment, when available, to help ensure that the noise impact of the development on itself are maintained within acceptable levels. Outdoor sound emissions should also be checked to ensure compliance with the noise by-law.







Block No.	Acoustic Barrier	Ventilation Requirements*	Type of Warning Clause	Required STC
А		Central A/C	A, B	OBC
B		Central A/C	A, B	OBC

Notes:

* The location, installation and sound rating of the air conditioning condensers must be compliant with MOECC Guideline NPC-300 as applicable.

-- no specific requirement

LR/DR – Living Room/Dining Room

BR – Bedroom

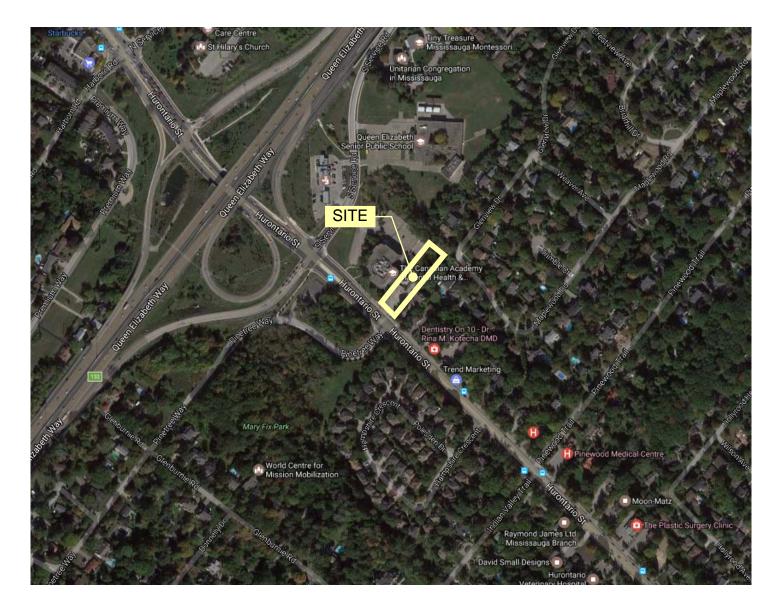
8.1 Implementation

To ensure that the noise control recommendations outlined above are fully implemented, it is recommended that:

- Prior to the issuance of building permits for this development, the Municipality's building inspector or a Professional Engineer qualified to perform acoustical engineering services in the Province of Ontario should certify that the noise control measures have been properly incorporated.
- Prior to assumption of the subdivision, the Municipality's building inspector or a Professional Engineer qualified to perform acoustical engineering services in the Province of Ontario should certify that the noise control measures have been properly incorporated, installed and constructed.















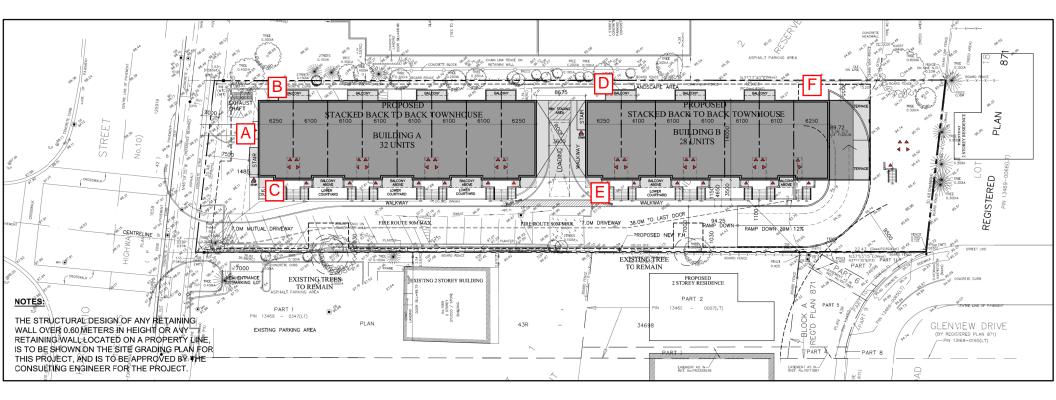


Figure 2 - Proposed Site Plan Showing Prediction Locations



LEGEND

Central air conditioning required

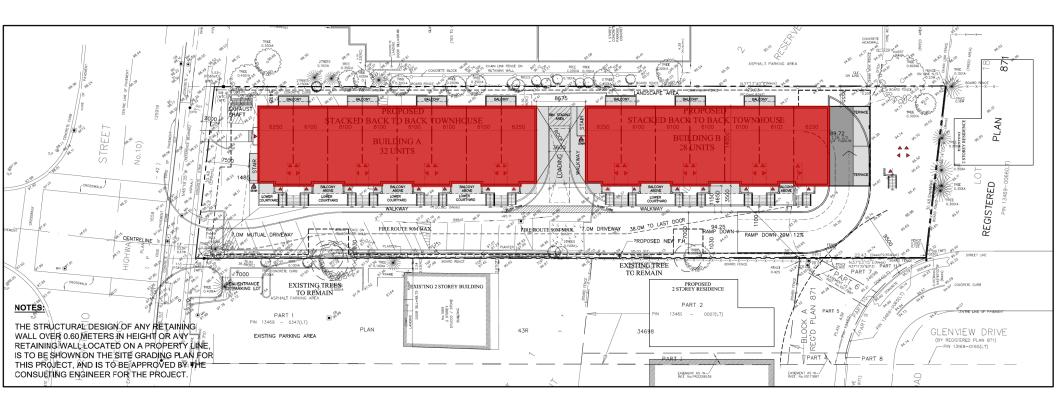


Figure 3 - Proposed Site Plan Showing Ventilation Requirements



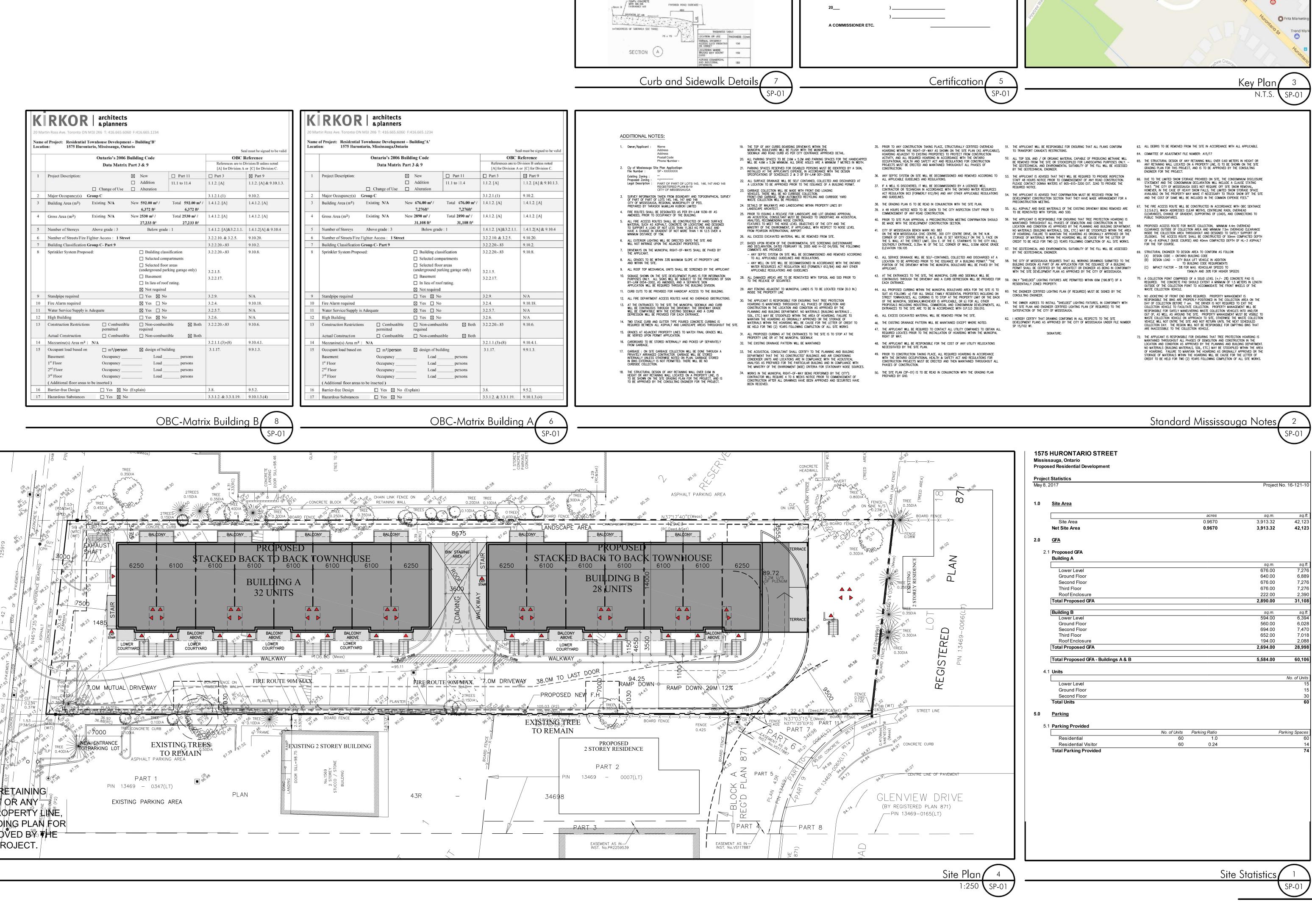
APPENDIX A

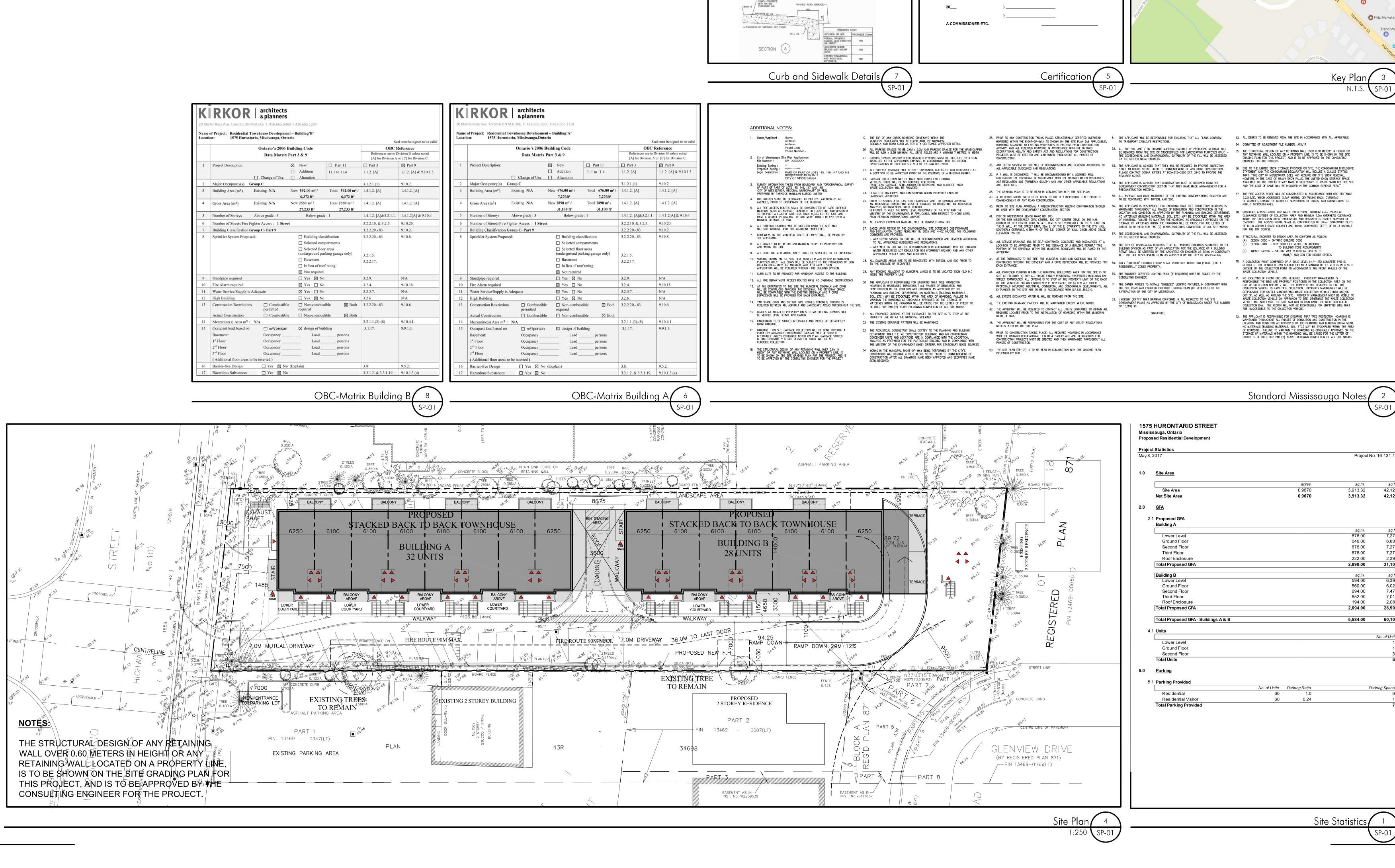
Supporting Drawings

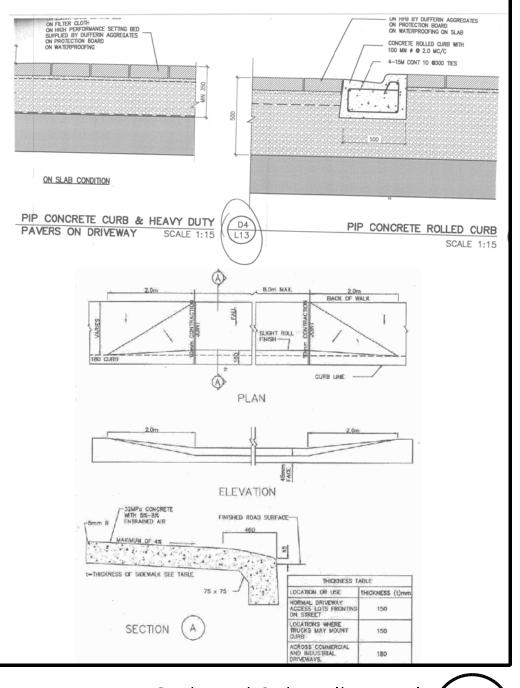




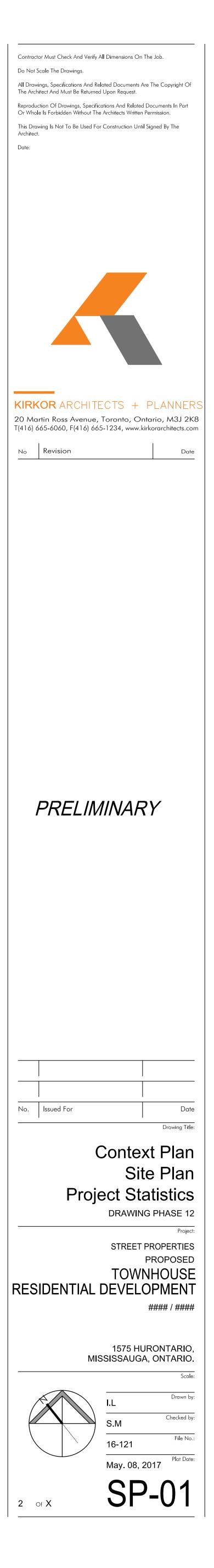


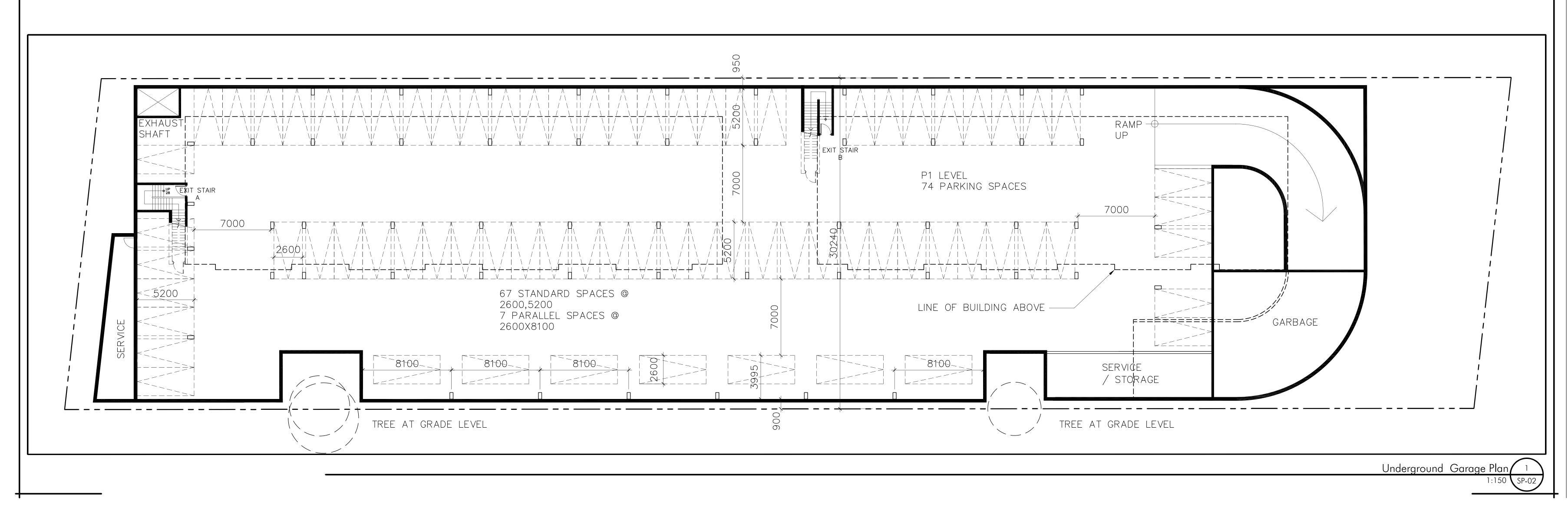


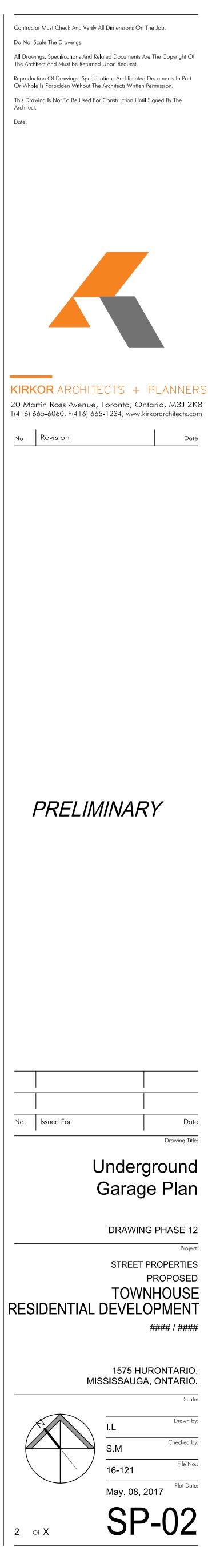


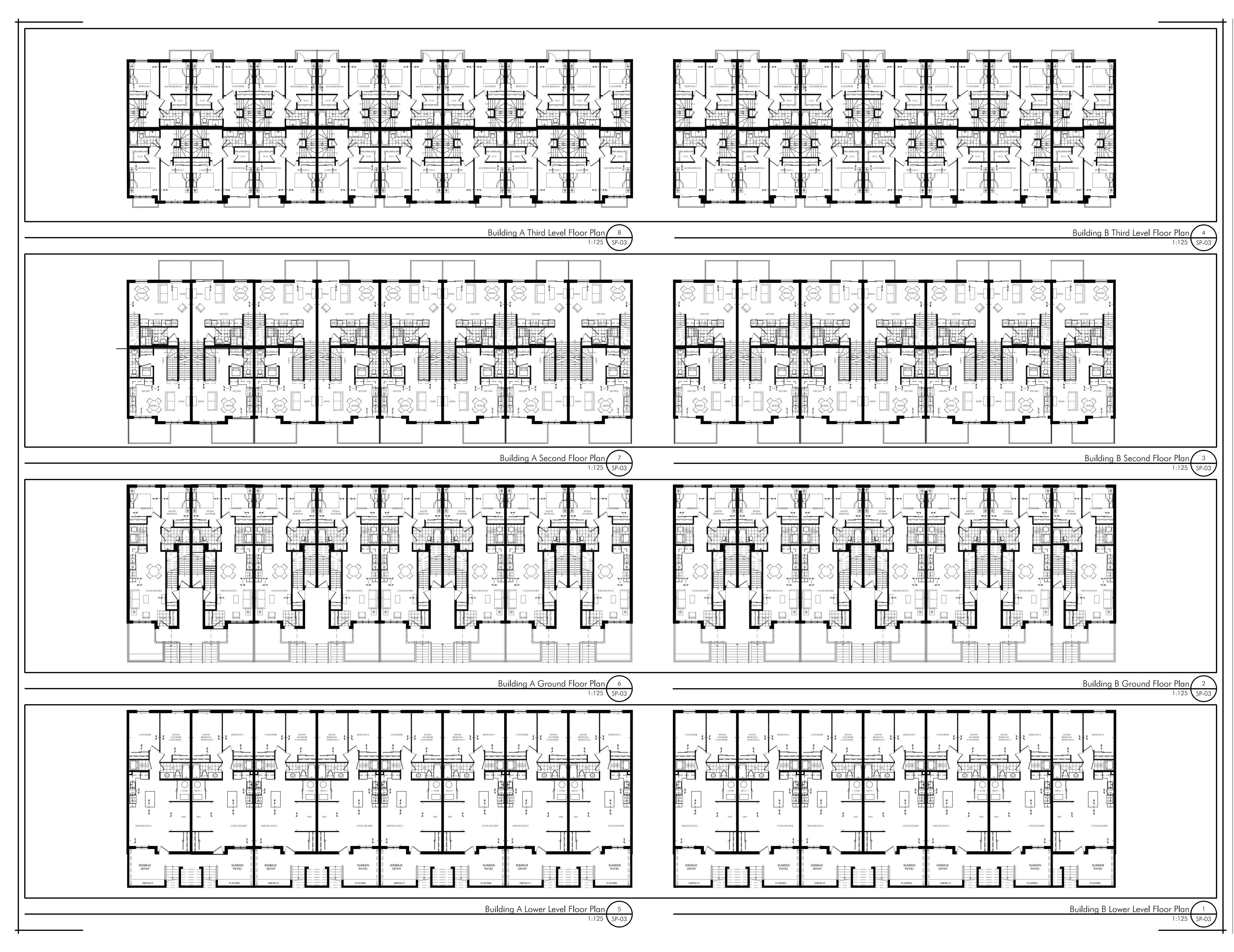


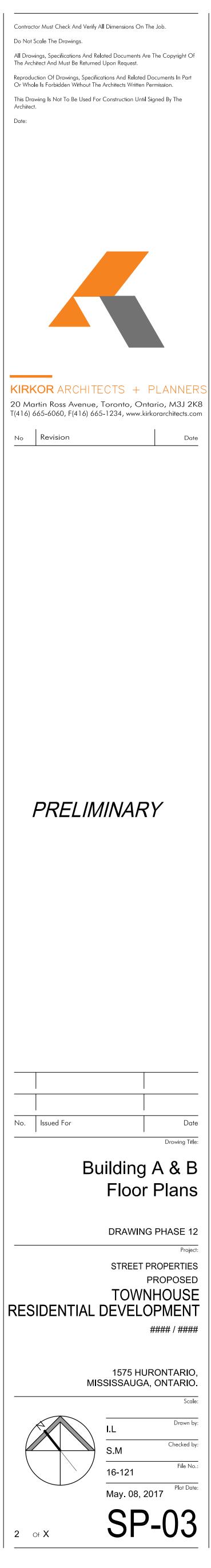
SIGNED CONDOMINIUM DECLARATIONS FOR MULTIPLE FAMILY RESIDENTIAL DEVELOPMENTS AS FOLLOWS: DOMINION OF CANADA) IN THE MATTER OF A PROVINCE OF ONTARIO) MULTIPLE RESIDENTIAL) BUILDING DEVELOPMENT REGIONAL MUNICIPALITY) ON PROPERTY LOCATED IN OF PEEL) THE CITY OF MISSISSAUGA	Ontario Provincial Police
) BEING KNOWN AS TO WIT:) PROPOSED 3 STOREY CONDOMINIUM BUILDING) 650 ATWATER AVENUE LTD. I, MAKE OATH AND SAY AS FOLLOWS:	1 Hurontario St
 I AM THE PRESIDENT OF SIERRA BUILDING GROUP. WHICH IS THE OWNER AND BUILDER OF 3 STOREY CONDOMINIUM BUILDING ON PROPERTY DESCRIBED ABOVE. THAT THE SAID MULTIPLE RESIDENTIAL BUILDING IS BEING BUILT TO BE SOLD 	
AS CONDOMINIUM APARTMENTS AND I MAKE THIS SOLEMN DECLARATION CONSCIENTIOUSLY BELIEVING IT TO BE TRUE AND KNOWING THAT IT IS OF THE SAME FORCE AND EFFECT AS IF I MAKE IT UNDER OATH.	Affinity Systems The Car of Dest
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IN THE MUNICIPALITY OF)))	Pinetree Way
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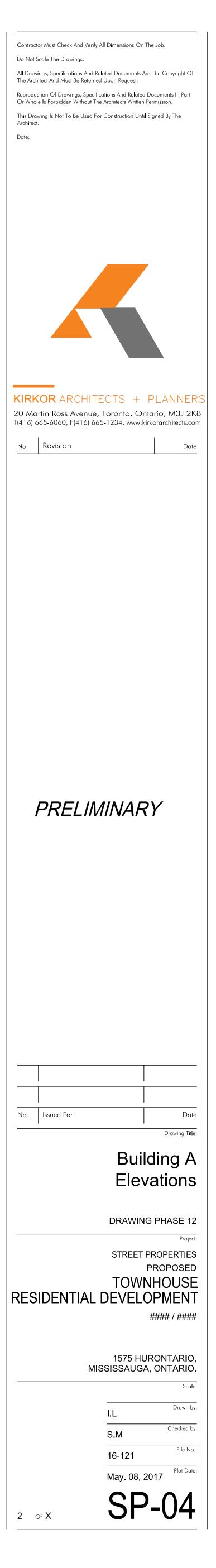


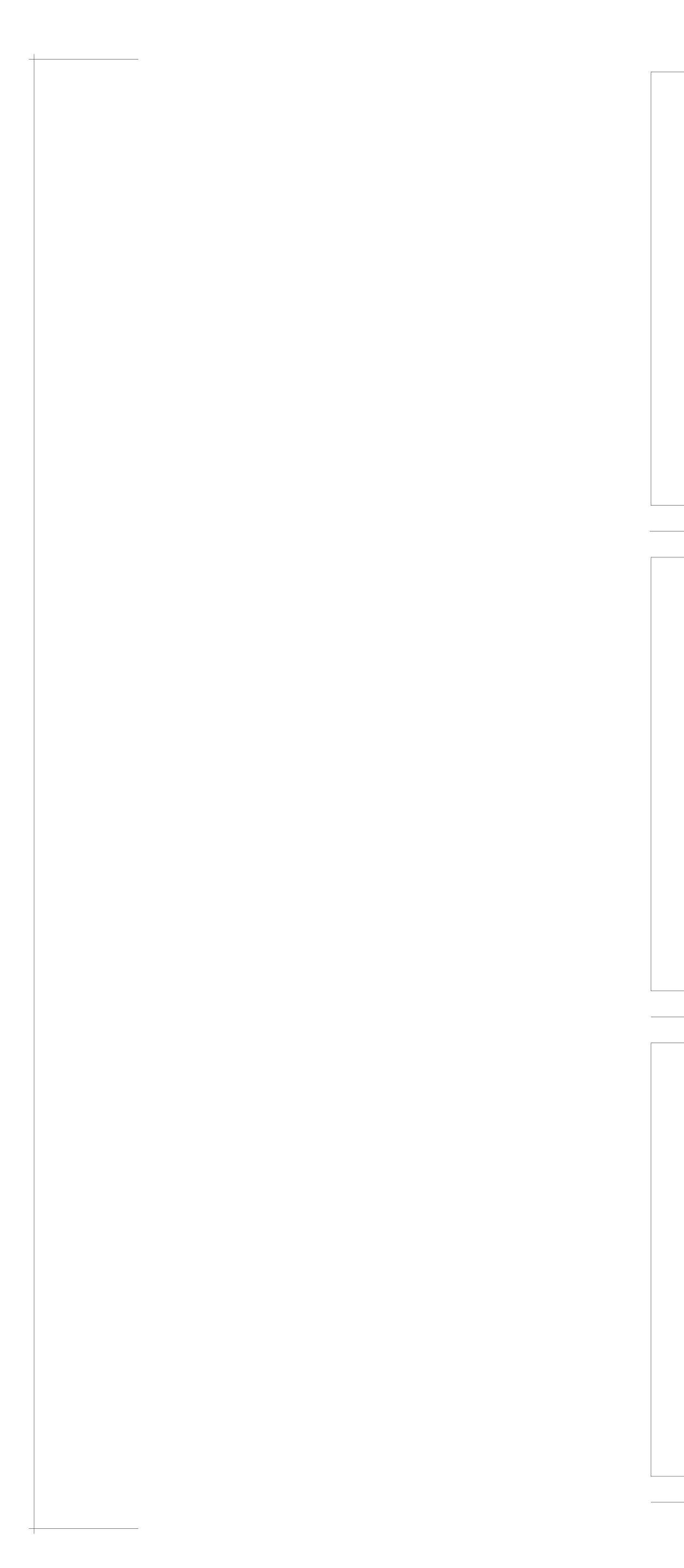








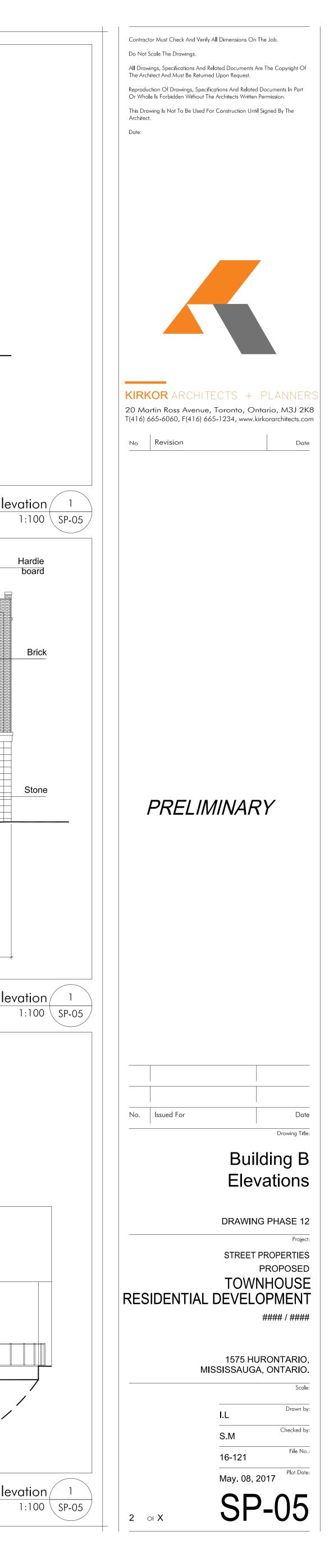












APPENDIX B

Road Traffic Information







Date:	2	23-Mar-17	NOISE REPORT FOR PROPOSED DEVELOPMENT					
	REQUESTED BY:							
Name: Victor Garcia								
Company	HGC Engineering		MISSISSAUGA					
		Location:	Hurontario Street (near 1575 Hurontario Street)					
	PREPARED BY:		Hurontario Street south of QEW					
Name:	Jacqueline Hunter							
ſel#:	(905) 615-3200	Look Up ID)#: 369					
		\mathbf{O}	N SITE TRAFFIC DATA					
	Specific	Hurontario Street	Street Names					
		48,000						
AADT:		40,000						
# of Lanes:		4						
% Trucks	Heavy Trucks Ratio:	55/45						
	t Traffic Split:	90/10						
	peed Limit:	50 km/h						
Gradient		<2%						
		35m						
Ultimate F	K U W:							
C	comments:	* Ultimate Traffic Dat	ta					
		AND AND AND A CONTRACT OF A DATA	ed on the proposed LRT project along Hurontario Street with existing lanes					
		converted from 6 to 4 lanes with 2 LRT lines in middle/both sides.						

Highway	Location Description	Dist. (KM)	Year	Pattern Type	AADT	SADT	SAWDT	WADT	AR
			2005	С	126,400	140,700	141,900	113,500	0.5
			2006	С	125,200	139,100	140,200	112,600	0.3
			2007	С	131,900	146,600	148,600	118,500	0.4
			2008	С	120,400	132,900	131,000	108,000	0.5
			2009	С	126,600	139,700	141,100	113,900	0.3
			2010	С	128,300	141,400	142,700	115,500	0.4
			2011	С			147,100		
			2012	С	134,000	147,400	144,700	120,600	N/A
			2013	С	135,500	149,000	147,600	121,900	N/A
QEW	MISSISSAUGA RD IC-130	2.0	1988	С	114,000	126,500	126,500	102,500	1.0
			1989	С			132,100		
			1990	С			134,900		
			1991	С			133,300		
			1992	С			134,100		
			1993	С			136,800		
			1994	С			140,900		
			1995	С			143,700		
			1996	С			150,400		
			1997	С			161,700		
			1998	С			168,600		
			1999	С			172,700		
			2000	С			164,800		
			2001	С			167,200		
			2002	С			169,300		
			2003	С			174,900		
			2004	С			178,500		
			2005	С			181,900		
			2006	С			170,800		
			2007	C			174,100		
			2008	С			149,300		
			2009	С			166,300		
			2010	C			176,500		
			2011	C			177,900		
			2012	C			174,800		
QEW	HWY 10-HURONTARIO ST IC-132	2.1	2013 1988	C C			163,500		
		2.1		C			138,400 143,200		
			1989			-		-	
		I	1990	С	130,900	140,000	151,700	124,300	1.0

Highway	Location Description	Dist. (KM)	Year	Pattern Type	AADT	SADT	SAWDT	WADT	AR
			1991	С	128,900	136,600	148,200	125,000	0.8
			1992	С	129,800	137,500	146,600	119,400	0.8
			1993	С	137,900	146,200	155,800	126,900	1.1
			1994	С	143,700	152,300	160,900	132,200	1.3
			1995	С	144,600	153,300	160,500	133,000	1.2
			1996	С	148,100	157,600	173,300	140,700	1.0
			1997	С	151,600	159,200	177,400	142,500	0.8
			1998	С	155,100	165,000	181,500	147,300	1.1
			1999	С	157,600	167,700	184,400	149,700	0.9
			2000	С	160,500	170,800	189,100	150,900	1.2
			2001	С	163,500	174,900	192,900	153,700	0.8
			2002	С	166,500	177,400	195,900	155,900	1.0
			2003	С	169,500	179,700	200,000	159,300	0.9
			2004	С			218,500		
			2005	С			205,100		
			2006	С			195,700		
			2007	С	169,000	179,200	195,600	158,600	1.1
			2008	С			154,600		
			2009	С			188,400		
			2010	С			193,000		
			2011	С			188,700		
			2012	С			182,600		
			2013	С			185,300		
QEW	CAWTHRA RD IC-134	1.8	1988	С			140,600		
			1989	С			145,400		
			1990	С			154,100		
			1991	С			150,500		
			1992	С			149,000		
			1993	С			157,900		
			1994	С			154,200		
			1995	С			155,000		
			1996	С		150,600		134,400	
			1997	С			167,800		
			1998	С			178,000		
			1999	С			178,500		
			2000	С			183,700		
			2001	С			187,900		
			2002	С	162,500	173,100	191,200	152,100	0.7

Victor Garcia

From:	Bee, Christopher (MTO) <christopher.bee@ontario.ca></christopher.bee@ontario.ca>
Sent:	March-28-17 12:52 PM
То:	Victor Garcia
Cc:	Jawed, Bushra (MTO); Bee, Christopher (MTO)
Subject:	RE: Commercial vehicle percent for QEW at Hurontario

To Victor Garcia, HGC Engineering:

QEW and Hurontario (Hwy 10) is at reference point LHRS 10150 Based on official MTO TVIS data, from years 2011 to 2013, the (% truck/commercial) at this location has increased slightly to 12.0%.

There is no official data after 2013.

Regards.

Christopher Bee MTO Central Region Traffic Office Safety Traffic Information and Roadwork Coordination Section (STIRCS)

From: Victor Garcia [mailto:vgarcia@hgcengineering.com]
Sent: March-23-17 10:29 AM
To: Jawed, Bushra (MTO)
Cc: Bee, Christopher (MTO)
Subject: Commercial vehicle percent for QEW at Hurontario

Hi Bushra,

HGC Engineering is performing a Noise Feasibility Study for a proposed stacked townhouse development located at 1575 Hurontario Street in the City of Mississauga. A google link is included for your reference:

https://goo.gl/maps/v3juL1Z6SaT2

We previously obtained the attached commercial vehicle percentage in the area. Are these numbers still valid?

Thanks,

Victor Garcia, P.Eng Project Engineer

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APPENDIX C

Sample STAMSON 5.04 Output







B. TXT Date: 16-08-2017 10:27:53 NORMAL REPORT STAMSON 5.0 MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT Time Period: Day/Night 16/8 hours Filename: b.te Description: Building A, north facade Road data, segment # 1: Hurontario (day/night) Car traffic volume : 19440/2160 veh/TimePeriod * Medium truck volume : 1188/132 veh/TimePeriod 972/108 veh/TimePeriod * Heavy truck volume : 50 km/h Posted speed limit Road gradient 0 % Road pavement 1 (Typical asphalt or concrete) * Refers to calculated road volumes based on the following input: 24 hr Traffic Volume (AADT or SADT): Percentage of Annual Growth : 24000 0.00 Number of Years of Growth 0.00 Medium Truck % of Total Volume Heavy Truck % of Total Volume 5.50 4.50 Day (16 hrs) % of Total Volume 90.00 Data for Segment # 1: Hurontario (day/night) Angl e2 Angl e1 -90.00 deg 0.00 deg Wood depth 0 (No woods.) No of house rows 0 / 0 Surface 2 (Reflective ground surface) 21.00 / 21.00 m Receiver source distance Receiver height 7.50 / 7.50 m (Flat/gentle slope; no barrier) Topography 1 0.00 Reference angle Road data, segment # 2: Hurontario (day/night) _ _ _ _ _ _ _ _ _ Car traffic volume : 19440/2160 veh/TimePeriod Medium truck volume : 1188/132 veh/TimePeriod * 972/108 veh/TimePeriod * Heavy truck volume : Posted speed limit : 50 km/h 0 % Road gradient Road pavement 1 (Typical asphalt or concrete) * Refers to calculated road volumes based on the following input: 24 hr Traffic Volume (AADT or SADT): 24000 Percentage of Annual Growth 0.00 Number of Years of Growth 0.00 Medium Truck % of Total Volume 5.50 Heavy Truck % of Total Volume 4.50 Day (16 hrs) % of Total Volume 90.00 Data for Segment # 2: Hurontario (day/night) -90.00 deg Angl e1 0.00 deg Angl e2 Wood depth (No woods.) 0 No of house rows 0 / 0 (Reflective ground surface) Surface 2 31.00 / 31.00 m Receiver source distance Receiver height 7.50 / 7.50 m Page 1 *"*S"

ACOUSTICS

VIBRATION

NOISE

B. TXT Topography 1 (Flat/gentle slope; no barrier) Reference angle 0.00 Road data, segment # 3: QEW (day/night) _ _ _ _ _ _ _ _ _ _ Car traffic volume : 102308/13951 veh/TimePeriod Medium truck volume : 3488/476 veh/TimePeriod Heavy truck volume : 10463/1427 veh/TimePeriod Posted speed limit 100 km/h : 0 % Road gradient 1 (Typical asphalt or concrete) Road pavement * Refers to calculated road volumes based on the following input: 24 hr Traffic Volume (AADT or SADT): 93500 Percentage of Annual Growth 2.50 Number of Years of Growth 14.00 Medium Truck % of Total Volume 3.00 Heavy Truck % of Total Volume Day (16 hrs) % of Total Volume 9.00 88.00 Data for Segment # 3: QEW (day/night) Angle1 Angle2 : -90.00 deg 90.00 deg Wood depth 0 (No woods.) No of house rows 1/1 House density 50 % Surface (Absorptive ground surface) 1 : 263.00 / 263.00 m : 7.50 / 7.50 m Receiver source distance Receiver height (Flat/gentle slope; no barrier) Topography 1 Reference angle 0.00 Road data, segment # 4: QEW (day/night) Car traffic volume : 102308/13951 veh/TimePeriod Medium truck volume : 3488/476 veh/TimePeriod Heavy truck volume : 10463/1427 veh/TimePeriod 100 km/h Posted speed limit : 0 % Road gradient Road pavement 1 (Typical asphalt or concrete) * Refers to calculated road volumes based on the following input: 24 hr Traffic Volume (AADT or SADT): 93500 Percentage of Annual Growth Number of Years of Growth 2.50 14.00 Medium Truck % of Total Volume Heavy Truck % of Total Volume 3.00 9.00 Day (16 hrs) % of Total Volume 88.00 Data for Segment # 4: QEW (day/night) -90.00 dea Angl e1 Angle2 90.00 deg Wood depth 0 (No woods.) No of house rows 1 / 50 % House density (Absorptive ground surface) Surface 1 Receiver source distance : 286.00 / 286.00 m Receiver height 7.50 / 7.50 : m (Flat/gentle slope; no barrier) Topography 1 Reference angle : 0.00





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*"*S"

VIBRATION

B. TXT Results segment # 1: Hurontario (day) Source height = 1.46 mROAD (0.00 + 65.49 + 0.00) = 65.49 dBAAngle1 Angle2 Alpha RefLeq P. Adj D. Adj F. Adj W. Adj H. Adj B. Adj SubLeq -90 0 0.00 69.96 0.00 -1.46 -3.01 0.00 0.00 0.00 65.49 _ _ _ _ _ _ _ _ _ Segment Leq : 65.49 dBA Results segment # 2: Hurontario (day) Source height = 1.46 m ROAD (0.00 + 63.80 + 0.00) = 63.80 dBAAnglel Angle2 Alpha RefLéq P. Adj D. Adj F. Adj W. Adj H. Adj B. Adj SubLeq -90 0 0.00 69.96 0.00 -3.15 -3.01 0.00 0.00 0.00 63.80 _____ Segment Leq : 63.80 dBA Results segment # 3: QEW (day) ------Source height = 1.73 m ROAD (0.00 + 62.57 + 0.00) = 62.57 dBAAngle1 Angle2 Alpha RefLeq P. Adj D. Adj F. Adj W. Adj H. Adj B. Adj SubLeq -90 90 0.47 84.51 0.00 -18.32 -1.12 0.00 -2.49 0.00 62.57 _____ Segment Leq : 62.57 dBA Results segment # 4: QEW (day) ------Source height = 1.73 m ROAD (0.00 + 62.05 + 0.00) = 62.05 dBAAngle1 Angle2 Alpha RefLeq P. Adj D. Adj F. Adj W. Adj H. Adj B. Adj SubLeq -90 90 0.47 84.51 0.00 -18.86 -1.12 0.00 -2.48 0.00 62.05 _____ Segment Leq : 62.05 dBA Total Leq ALI Segments: 69.71 dBA 9 Results segment # 1: Hurontario (night) Source height = 1.46 mROAD (0.00 + 58.96 + 0.00) = 58.96 dBAAnglel Angle2 Alpha RefLéq P. Adj D. Adj F. Adj W. Adj H. Adj B. Adj SubLeq Page 3 ري گ

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VIBRATION

B. TXT -90 0 0.00 63.43 0.00 -1.46 -3.01 0.00 0.00 0.00 58.96 _____ Segment Leq : 58.96 dBA Results segment # 2: Hurontario (night) Source height = 1.46 mROAD (0.00 + 57.26 + 0.00) = 57.26 dBAAngle1 Angle2 Alpha RefLeq P. Adj D. Adj F. Adj W. Adj H. Adj B. Adj SubLeq -90 0 0.00 63.43 0.00 -3.15 -3.01 0.00 0.00 0.00 57.26 _ _ _ _ _ _ _ _ _ Segment Leq : 57.26 dBA Results segment # 3: QEW (night) Source height = 1.73 mROAD (0.00 + 56.93 + 0.00) = 56.93 dBAAngle1 Angle2 Alpha RefLeq P. Adj D. Adj F. Adj W. Adj H. Adj B. Adj SubLeq -90 90 0.47 78.87 0.00 -18.32 -1.12 0.00 -2.49 0.00 56.93 Segment Leq : 56.93 dBA Results segment # 4: QEW (night) Source height = 1.73 m_ _ _ _ _ _ _ _ _ _ -90 90 0.47 78.87 0.00 -18.86 -1.12 0.00 -2.48 0.00 56.41 _____ Segment Leg : 56.41 dBA Total Leq All Segments: 63.52 dBA TOTAL Leq FROM ALL SOURCES (DAY): 69.71 dBA (NIGHT): 63.52 dBA







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VIBRATION