

September 2018

UD17-094

Functional Servicing and

Stormwater Management Report (Phase I)







Project: 1444-1458 Cawthra Road

2530173 Ontario Corporation

Lithos Group Inc. 150 Bermondsey Road Toronto, ON M4A-1Y1 Tel: (416) 750-7769

Email: info@LithosGroup.ca

PREPARED BY:

Angelos Andreadis, P.E., M.A.Sc., Project Design Manager

REVIEWED BY:



Nick Moutzouris, P.Eng., M.A.Sc.

Principal

LITHOS GROUP INC.

Issues and Revisions Registry

Identification	Date	Description of issued and/or revision
Functional Servicing and Stormwater Management Report (Phase I)	September 28 th , 2018	Issued for Rezoning Application

Functional Servicing and Stormwater Management Report (Phase I)

Statement of Conditions

This Report / Study (the "Work") has been prepared at the request of, and for the exclusive use of, the Owner / Client, the City of Mississauga and its affiliates (the "Intended User"). No one other than the Intended User has the right to use and rely on the Work without first obtaining the written authorization of Lithos Group Inc. and its Owner. Lithos Group Inc. expressly excludes liability to any party except the intended User for any use of, and/or reliance upon, the work.

Neither possession of the Work, nor a copy of it, carries the right of publication. All copyright in the Work is reserved to Lithos Group Inc. The Work shall not be disclosed, produced or reproduced, quoted from, or referred to, in whole or in part, or published in any manner, without the express written consent of Lithos Group Inc. and the Owner.

Executive Summary

Lithos Group Inc. (Lithos) was retained by 2530173 Ontario Corporation (the "Owner") to prepare a Functional Servicing and Stormwater Management (FSR-SWM) Report (Phase I), in support of a Rezoning Application, for a proposed residential use development to be located at 1444-1458 Cawthra Road, in the City of Mississauga (the "City"). The following summarizes our conclusions:

Storm Drainage

More details for the Stormwater Management (SWM) Section of this report will be prepared at the Site Plan Application stage (Phase II). The site stormwater discharge will be controlled to the 2-year predevelopment flow and will be connected to the existing 1050 mm diameter storm sewer on Cawthra Road. In order to achieve the target flows and meet the City's Storm Water Quantity Control requirements, quantity controls will be utilized and up to 110.9 m³ of storage will be required. The stormwater management (SWM) system will be designed to provide enhanced level (Level 3) protection as specified by the Ministry of Environment and Climate Change (MOECC). During Site Plan Application, a detailed analysis will be provided to assess the water quality on site and determine additional measures in order to achieve a minimum total suspended solids (TSS) removal of 80%.

Sanitary Sewers

Sixteen (16) separate ownerships will comprise the proposed development, one for each townhouse unit and one for each detached dwelling. In order to provide separate connection for each residential dwelling and townhouse development, an easement will be incorporated during the detailed design stage. The proposed development, will connect to the existing 250 mm sanitary sewer on Cawthra Road, via a 150mm diameter sanitary lateral. The additional net discharge flow from the proposed buildings, is anticipated at approximately 0.70 L/s, which represents less than 1% of the full flow capacity of the existing 250mm diameter sanitary sewer along Cawthra Road, therefore it is considered negligible. Following that fact, the existing infrastructure can support the proposed development.

Water Supply

The proposed development will be comprised by sixteen (16) separate ownerships. Similarly to sanitary connections, each ownership will connect to the proposed water service which will be located within the proposed easement. The proposed water service will connect to the existing 300 mm diameter watermain located on the south side of Cawthra Road. It is anticipated that a total design flow of 83.42 L/s will be required to support the proposed development. The results of the hydrant flow test reveal the existing water infrastructure can support the proposed development.

Site Grading

The proposed grades will improve the existing drainage conditions to meet the City's/Regional requirements. Grades will be maintained along the property line wherever feasible and emergency overland flow will continue draining according to the existing draining pattern.

Table of Contents

1.0	Introduction	1
2.0	Site Description	1
3.0	Site Proposal	1
4.0	Terms of Reference and Methodology	2
	4.1. Terms of Reference	2
	4.2. Methodology: Stormwater Drainage and Management	2
	4.3. Methodology: Sanitary Discharge	2
	4.4. Methodology: Water Usage	3
5.0	Stormwater Management and Drainage	3
	5.1. Existing Conditions	3
	5.2. Stormwater Management	3
	5.2.1. Stormwater Runoff Volume Reduction	
	5.2.2. Quantity Controls	
	5.2.3. Quality Controls	
	5.3. Proposed Storm Connection	5
6.0	Sanitary Drainage System	5
	6.1. Existing Sanitary Drainage System	5
	6.2. Existing and Proposed Sanitary Flows	6
	6.3. Proposed Sanitary Connection	6
7.0	Water Supply System	6
	7.1. Existing System	6
	7.2. Proposed Water Supply Requirements	6
	7.3. Proposed Watermain Connection	7
8.0	Site Grading	7
	8.1. Existing Grades	7
	8.2. Proposed Grades	8
9.0	Conclusions and Recommendations	8

Functional Servicing and Stormwater Management Report (Phase I)

LIST OF FIGURES

Figure 1 - Location Plan

Figure 2 - Aerial Plan

LIST OF TABLES

Гable 4.1 – Sanitary Flows	2
Fable 4.2 – Water Usage	
Гable 5.1 – Target Input Parameters	
Table 5.2 – Target Peak Flows	
Table 5.3 – Post-development Input Parameters	
Fable 5.4 – Post-development Quantity Control as per City Requirements	
Table 7.1 – Fire Flow Input Parameters	7

APPENDICES

Appendix A – Site Photographs

Appendix B – Background Information

Appendix C – Storm Analysis

Appendix D – Sanitary Data Analysis

Appendix E – Water Data Analysis

1.0 Introduction

Lithos Group Inc. (Lithos) was retained by 2530173 Ontario Corporation (the "Owner") to prepare a Functional Servicing and Stormwater Management Report (Phase I), in support of Rezoning Application for a proposed residential development, located at 1444-1458 Cawthra Road in the City of Mississauga (City).

The purpose of this report is to provide site-specific information for the City's review with respect to infrastructure required to support the proposed development. More specifically, the report will present details on sanitary discharge, water supply and an outline of the storm pattern.

We contacted the City's engineering department to obtain existing information in preparation of this report. The following documents were available for our review:

- Plan and profile drawings of Cawthra Road, Drainage and Utilities, drawing No.
 - 8313 D, dated May 1985;
 - o 8315 D, dated May 1985;
 - 8325 D, dated May 1985;
 - C 5966, dated March 1963;
- Site Plan and Statistics prepared by KFA Architects and Planners Inc., dated September 28, 2018;
 and,
- Topographical Survey prepared by Tom A. Senkus, dated March 30, 2017.

2.0 Site Description

The existing site is approximately 0.536 hectares of residential-use land. It is currently occupied by four (4) detached residential dwellings, outdoor paved parking area and landscaped area, as indicated by the topographic survey in **Appendix B**. The site is bound by Cawthra Road to the north and residential dwellings to the south, east and west. Refer to **Figures 1** and **2** following this report and site photographs in **Appendix A**.

3.0 Site Proposal

The proposed development will include four (4) blocks of two-storey stacked townhouses as well as four (4) two-storey detached residential dwellings and it will be comprised of sixteen (16) ownerships, one for each of the proposed townhouses and single residential dwellings. The proposed development will include approximately a total 3,642 m² of Gross Floor Area (GFA). Please refer to **Appendix B** for the proposed site plan and site statistics.

Note that there is approximate portion of 0.03 ha on the north side of the property, which will be conveyed to the City (future extension of Cawthra Road). Therefore, the future private property will be 0.506 ha. Please refer to **Appendix B** for the proposed site plan and site statistics.

4.0 Terms of Reference and Methodology

4.1. Terms of Reference

The Terms of Reference used for the scope of this report were based on:

- City of Mississauga Development Requirements Manual, revised September 2016;
- Region of Peel Watermain Design Criteria, revised June 2010;
- Region of Peel Sanitary Sewer Design Criteria, revised March 2017;
- Ministry of Environment: Guidelines for the Design of Sanitary Sewage Works 2008;
- Ministry of Environment: Design Guidelines for Drinking Water Systems 2008;
- Ministry of Environment: Stormwater Management Planning and Design Manual 2003; and
- Ontario Building Code 2012 (O.B.C.)

4.2. Methodology: Stormwater Drainage and Management

This report provides an overview of the pre and post-development conditions, and comments on opportunities to reduce peak flows. A detailed Stormwater Management (SWM) report will be prepared at the Site Plan Application Stage (Phase II).

The proposed development will be designed to meet the Region's and the standards of the Province of Ontario as set out in the Ministry of Environment and Climate Change (MOECC) 2003 Stormwater Management Planning and Design Manual (SWMPD). The following design criteria will be reviewed:

- Post-development peak flow for the 100-year from the site should be controlled to the two (2)-year target flow according to the Credit Valley Conservation (CVC);
- A specified rainfall depth of 5 mm is to be retained on-site as required by the City of Mississauga Development Requirements Manual for stormwater runoff volume reduction;
- A safe overland flow will be provided for all flows in excess of the 100-year storm event.

4.3. Methodology: Sanitary Discharge

The sanitary sewage discharge from the site will be determined using sanitary sewer design sheets that incorporate the land use and building statistics as supplied by the design team. The calculated values provide peak sanitary flow discharge that considers infiltration.

The estimated sanitary discharge flows from the proposed site will be calculated based on the criteria shown in **Table 4.1.**

Table 4.1 – Sanitary Flows

Usage	Design Flow	Units	Population Equivalent
Residential	302.8	Litres / capita / day	Single Family = 50 people / ha

Based on the calculated peak flows, the adequacy of the existing infrastructure to support the proposed development will be discussed.

Methodology: Water Usage 4.4.

The domestic water usage was calculated based on the City's design criteria outlined in **Table 4.2**.

Table 4.2 – Water Usage

Usage	Water Demand	Units
Typical Residential Water Demand	280	Litres / capita / day

Pressure and flow testing has been conducted on the existing hydrants located near the site along Cawthra Road to obtain existing flows, residual and static pressure.

Stormwater Management and Drainage 5.0

5.1. **Existing Conditions**

According to available records, there is an existing 1050 mm diameter storm sewer along Cawthra Road running south-east. The existing site drains partially uncontrolled towards the adjacent Cawthra Road and partially towards the rear yards, south-west of the existing dwellings.

The existing site is primarily undeveloped with a run-off coefficient estimated at 0.40. Table 5.1 shows the input parameters which are illustrated on the pre-development drainage area plan in Figure DAP-1 in Appendix C.

Table 5.1 – Target Input Parameters

Catchment	Drainage Area (ha)	С	Tc (min.)
A1 Pre	0.506	0.40	15

Peak flows calculated for the existing conditions are shown in Table 5.2 below. Detailed calculations are in Appendix C.

Table 5.2 – Target Peak Flows

	Peak Flow Rational Method				
Catchment	(L/s)				
	2-year	5-year	10-year	100-year	
A1 Pre	33.7	45.3	55.8	79.1	

As shown in Table 5.2, the post-development flows will need to be controlled to the target flow of 33.7 L/s.

5.2. **Stormwater Management**

In order to meet the City's Storm Design requirements, the development flow rate is to be controlled to the two (2)-year target flow established in **Section 5.1**.

The site has been separated into two (2) internal drainage areas:

- 1. A1 Post Storm runoff from the rooftops, the driveway area and the landscape areas, retained on-site, and eventually discharged into the existing 1050 mm diameter storm sewer in Cawthra Road.
- 2. A2 Post Uncontrolled storm runoff from the north portion of the site, flowing towards Cawthra Road.

The post-development drainage areas and runoff coefficients are indicated on Figure DAP-2, located in Appendix C and summarized in Table 5.3 below.

Drainage Area	Drainage Area inage Area (ha)		Runoff Coefficient for 100-Year Return Period "c"	Tc (min.)
A1 Post	0.455	0.61	0.76	15
A2 Post	0.051	0.30	0.37	15

Table 5.3 – Post-development Input Parameters

As per City's stormwater management guidelines, in order to account for increase in storm runoff due to saturation of the catchment surface, an adjustment factor of 1.25 will be used for the 100-year storm.

5.2.1. Stormwater Runoff Volume Reduction

As required by the City's guidelines, a rainfall depth of 5 mm must be retained over the entire parcel area. A 5 mm rainfall over the entire site equates to a required water balance volume of 25.31 m³. In order to achieve this, the following low impact development (LID) techniques will may be implemented.

- Soakway pit to infiltrate roof runoff;
- Permeable materials/Infiltration galleries/trenches to infiltrate surface runoff;
- Reuse for irrigation purposes;
- Rainwater barrels and/or tank;

Detailed calculations will be provided during the detailed design stage of Site Plan Application (Phase II).

5.2.2. Quantity Controls

Using the City's intensity-duration-frequency (IDF) data, modified rational method calculations were undertaken to determine the maximum storage required during each storm event. Results for the 2, 5, 10 and 100-year storm events are provided in Table 5.4 below. The detailed post-development quantity control calculations are provided in **Appendix C**.

Table 31-1	rable 514 1 65t development Quantity Control as per city hequitements				
Drainage Areas	Storm Event	Target Flow (L/s)	Required Storage Tank Volume (m³)		
A1 Post (Controlled)	2-year		18.1		
	5-year	22.7	32.4		
	10-year	33.7	45.6		
	100-year		110.9		

Table 5.4 – Post-development Quantity Control as per City Requirements

According to the City's Guidelines and Credit Valley Conservation (CVC) Watershed Boundaries the proposed development is located within Cawthra Creek Subwatershed, therefore the 100-year post runoff will be controlled to the 2-year pre-development condition. Watershed Boundaries can be found in **Appendix B**.

As shown in **Table 5.4**, in order to control post-development flows to 2-year pre-development conditions, a target flow of 33.7 L/s is to be satisfied. The minimum required on-site storage is 110.9 m². This can be achieved through the design and installation of stormwater holding tanks, flow control devices and/or parking ponding, underground chambers and infiltration trenches. Details will be provided through the detailed design stage of Site Plan Application (Phase II).

5.2.3. Quality Controls

Stormwater treatment must meet Enhanced Protection criteria as defined by the MOE 2003 SWMPD Manual, including a minimum 80% of total suspended solids removal (TSS). Water quality control can be provided by the rooftop/terraces and by an oil-grit separator (OGS) that will be required for the driveway area which will be exposed to oil and grit.

More details regarding sizing of the OGS and the total quality control achieved for the total site, will be provided through the detailed design stage of Site Plan Application (Phase II).

5.3. Proposed Storm Connection

The storm sewer system will be designed to meet the City's Storm requirements and discharge into the existing 1050 mm diameter storm sewer on Cawthra Road via a 200 mm diameter storm sewer service connection with a minimum grade of 2.00% (or equivalent design). The post-development 100-year storm will be designed to match the two (2)-year pre-development storm. Therefore, this development will not adversely affect flow conditions downstream and the existing infrastructure on Cawthra Road will be adequate to service this development. Refer to engineering drawing "SS-01" (submitted separately) indicating the stormwater service connection.

6.0 Sanitary Drainage System

6.1. Existing Sanitary Drainage System

The existing site is currently occupied by four (4) residential dwellings, outdoor paved parking area and landscaped area. According to available records there is an existing 250mm diameter sanitary sewer fronting the property along Cawthra Road running south-east.

6.2. Existing and Proposed Sanitary Flows

The sanitary flow generated by the proposed residential use development at 1444-1458 Cawthra Road was compared to the existing flow in order to quantify the net increase in the sanitary sewer.

Using the design criteria outlined in **Section 4.3** and existing site information, the sanitary discharge flow from the existing residential dwellings is estimated at 0.14 L/s. Detailed calculations can be found in **Appendix D**.

Similarly, using the design criteria and the proposed development statistics, the new development will discharge 0.84 L/s into the City's infrastructure.

The additional flow will be considered within the sanitary discharge rate, therefore, there is an increase in sanitary flow of approximately 0.70 L/s, which represents less than 1% of the full flow capacity of the existing 250mm diameter sanitary sewer along Cawthra Road, therefore it is considered negligible. Following that fact, the existing infrastructure can support the proposed development.

6.3. Proposed Sanitary Connection

Sixteen (16) separate ownerships will comprise the proposed development, one for each townhouse unit and one for each detached residential dwelling. In order to provide separate connection for each residential dwelling and townhouse development, an easement will be incorporated during the detailed design stage. Each ownership will connect into a proposed 150mm diameter sanitary sewer within the easement, which will discharge into the existing 250mm diameter sanitary sewer on the south side of Cawthra Road, at a minimum grade of 2.00% (or equivalent pipe design). Refer to engineering drawing "SS-01" (submitted separately) for details.

7.0 Water Supply System

7.1. Existing System

The existing watermain system consists of a 300 mm diameter watermain on the south side of Cawthra Road. Hydrant flow tests were carried out by Cole Engineering on April 11, 2018 along Cawthra Road Trail, to determine the flow and pressure in the existing water.

The results of the test indicate the existing static pressure is 441 KPa (64 psi) and 123.0 L/sec (1950 USPGM) of water is available with a residual pressure of 400 KPa (58 psi). The full detailed report is included in **Appendix E**.

7.2. Proposed Water Supply Requirements

The estimated water consumption was calculated based on the occupancy rates shown on **Table 4.2**, based on the Region's Watermain Design Criteria, revised June 2010. It is anticipated that an average consumption of approximately 0.14 L/s (12,096 L/day), a maximum daily consumption of 0.29 L/s (25,056 L/day) and a peak hourly demand of 0.43 L/s (1,548 L/hr) will be required to service this development with domestic water. Detailed calculations can be found in **Appendix E**.

The fire flow requirements we estimated using the method prescribed by the Fire Underwriters Survey (FUS) be undertaken to assess the minimum requirement for fire suppression. The fire flow calculation is normally conducted for the largest storey, by area, and for the two immediately adjacent storeys.

For this development, we have selected the worst case scenario for townhouse fire separation of 600m²/townhouse unit, according to the OBC requirements which translates to an equal separation of 200m²/floor for the three storey townhouse units. **Table 7.1** illustrates the input parameters used for the FUS calculations. According to our calculations, a minimum fire suppression flow of approximately 83.13 L/s (1,317 USGPM) will be required. Refer to detailed calculations found in **Appendix E**.

Table 7.1 – Fire Flow Input Parameters

				Separation Distance			
Davamatav	Frame used	Combustibility	Presence				
Parameter	for Building	of Contents	of Sprinklers	North	West	South	East
Value according to FUS options	Ordinary Construction	Non- Combustible	No	10.1m- 20m	0.0m- 3.0m	20.0m- 3.0m	20.1m- 30m
Surcharge/reduction from base flow	1.0	25%	0%	15%	25%	25%	10%

In summary, the required design flow is the sum of 'the minimum fire suppression flow' and 'maximum daily demand' (83.13+0.29 = 83.42 L/s, 1,322 USGPM).

The results of the hydrant flow test carried out by Cole Engineering on April 11, 2018 along Cawthra Road, indicate that 361.51 L/s (5750 USGPM) of water is available with a pressure of 138KPa (20.0 psi) revealing that the existing water infrastructure will support the proposed development. The hydrant flow tests can be found in **Appendix E**.

7.3. Proposed Watermain Connection

Sixteen (16) separate ownerships will comprise the proposed development, one for each townhouse unit and one for each detached residential dwelling. Similarly to sanitary connections, each ownership will connect to the proposed municipal water service which will be located within a proposed easement (to be provided during detailed design stage).

The proposed municipal water service will connect to the existing 300 mm diameter watermain located on the south side of Cawthra Road. Proposed townhouse developments residential dwellings will be serviced by 25mm diameter domestic services. For details, refer to engineering drawing "SS-01" (submitted separately).

8.0 Site Grading

8.1. Existing Grades

The existing property is currently occupied by four (4) residential dwellings, outdoor paved parking area and landscaped area. The existing site drains uncontrolled partially towards Cawthra Road and partially towards the rear yards, south-west of the existing dwellings.

8.2. Proposed Grades

The proposed grades will improve the existing drainage patterns wherever feasible. Grades will be maintained along the property line to the extent possible.

Stormwater consisting of the Cawthra Road access driveway, rooftops and the adjacent landscape area will be directed towards the underground storm tank and then discharged into the City's network. Overland flow for the proposed development will be maintained as is, however stormwater drainage conditions will be improved, due to the stormwater quantity controls described in **Section 5.2.2.**

9.0 Conclusions and Recommendations

Based on our investigations, we conclude the following:

Storm Drainage

More details for the Stormwater Management (SWM) Section of this report will be prepared at the Site Plan Application stage (Phase II). The site stormwater discharge will be controlled to the 2-year predevelopment flow and will be connected to the existing 1050 mm diameter storm sewer on Cawthra Road. In order to achieve the target flows and meet the City's Storm Water Quantity Control requirements, quantity controls will be utilized and up to 110.9 m³ of storage will be required. The stormwater management (SWM) system will be designed to provide enhanced level (Level 3) protection as specified by the Ministry of Environment and Climate Change (MOECC). During Site Plan Application, a detailed analysis will be provided to assess the water quality on site and determine additional measures in order to achieve a minimum total suspended solids (TSS) removal of 80%.

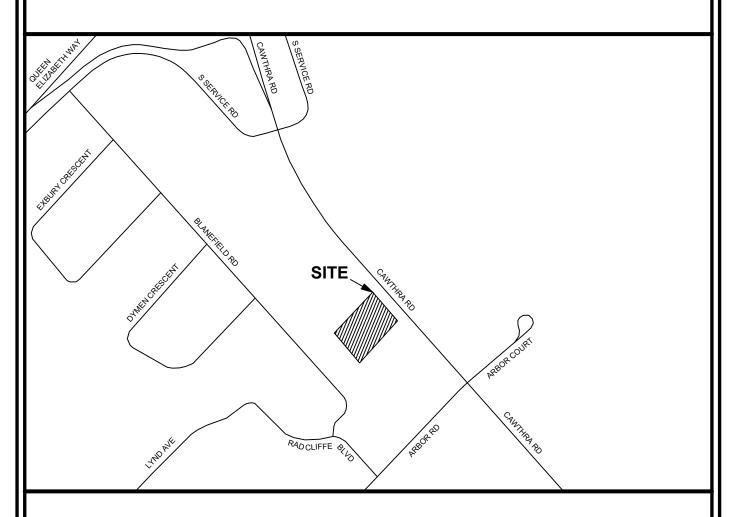
Sanitary Sewers

Sixteen (16) separate ownerships will comprise the proposed development, one for each townhouse unit and one for each detached dwelling. In order to provide separate connection for each residential dwelling and townhouse development, an easement will be incorporated during the detailed design stage. The proposed development, will connect to the existing 250 mm sanitary sewer on Cawthra Road, via a 150mm diameter sanitary lateral. The additional net discharge flow from the proposed buildings, is anticipated at approximately 0.70 L/s, which represents less than 1% of the full flow capacity of the existing 250mm diameter sanitary sewer along Cawthra Road, therefore it is considered negligible. Following that fact, the existing infrastructure can support the proposed development.

Water Supply

The proposed development will be comprised by sixteen (16) separate ownerships. Similarly to sanitary connections, each ownership will connect to the proposed water service which will be located within the proposed easement. The proposed water service will connect to the existing 300 mm diameter watermain located on the south side of Cawthra Road. It is anticipated that a total design flow of 83.42 L/s will be required to support the proposed development. The results of the hydrant flow test reveal the existing water infrastructure can support the proposed development.







LOCATION PLAN

RESIDENTIAL USE DEVELOPMENT 1444-1458 CAWTHRA ROAD MISSISSAUGA, ONTARIO

63-3-0	DATE:	SEP 2018	PROJECT No:	UD17-094
150 Bermonsdey Road, North York, Ontario M4A 1Y1	SCALE:	N.T.S.	FIGURE No:	FIG 1







AERIAL PLAN RESIDENTIAL USE DEVELOPMENT 1444-1458 CAWTHRA ROAD MISSISSAUGA, ONTARIO

	DATE:	SEP 2018	PROJECT No:	UD17-094
150 Bermonsdey Road, North York, Ontario M4A 1Y1	SCALE:	N.T.S.	FIGURE No:	FIG 2

APPENDIX A Site Photographs

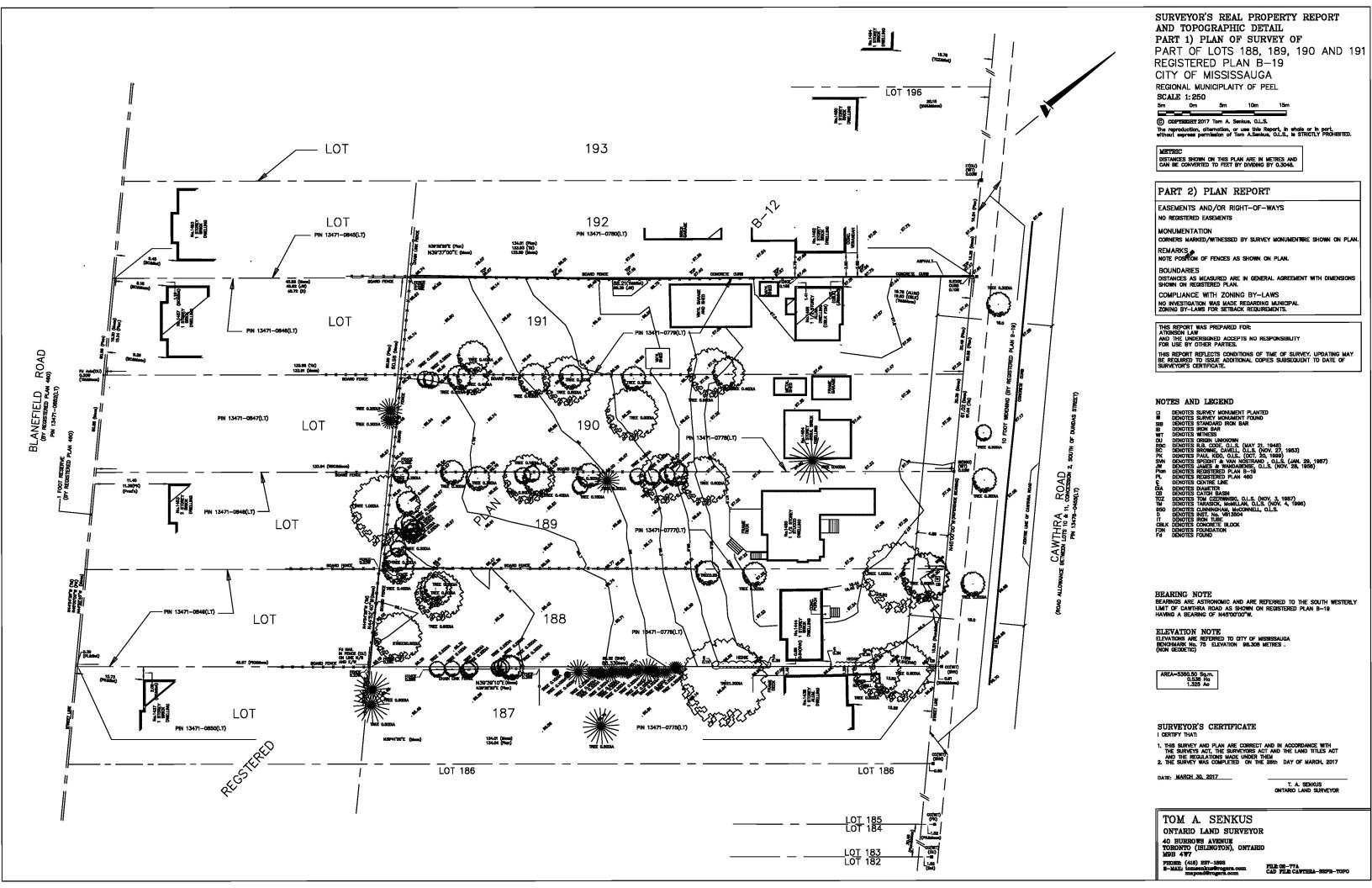


South-east Corner of property along Cawthra Road facing north



North-east Corner of property along Cawthra Road facing south

APPENDIX B Background Information









1444 1458

1444-1458 CAWTHRA ROAD MISSISSAUGA, ON

© Copyright KFA Architects and Planners Inc., all rights reserved. No part of this document whether printed form or supplied as digital data may be reproduced, stored in a retrieval system or transmitted in any form or by any means, mechanical photocopying, recording or otherwise without the prior written permission of KFA Architects and Planners Inc., All dimensions to be checked on site by the contractor, Drawings are not to be scaled, and any discrepancies are to be reported to the Architect

1	ssue to Consultants	2018,09,12
2	ssue for OP/RZ	2018,09,28

Context Plan

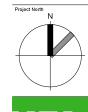
1: 1000

1444-1458		1					
			Date:	31-Aug-2018	Official Planning Designation	on: Residential Low	Density II
C	AWTHRA				Zoning By-law 0225-2007: F	R3-1	
KFA /	ARCHITECTS + PL	ANNERS	•				
Devel	opment Sta	atistics					
Site Area (a)				1	Site Area Breakdown Table	lm2)	Area
m ²	sq.ft	ha	acre		Paving		1214
5062.0	544887	0.51	1.25		Soft Landscaping Area		2259.0
		Units/Ha	Units/Acre		Hard Landscape Area		232.0
	L	32	13		Building Area (Combined La	argest Footprints)	1357.0
	General D	Development Stat	tisitics Table			Building He	inhts & Set
Total Number		CTCIOPIII.	institution (C.L.)	16.0	Block A	Height:	
Average Unit	Size Construc	ction Area (m²)		252.5	1	North	120000000000000000000000000000000000000
		ction Area (SF)		2718	Barrand Circ Code Code	East	
Gross Construction Area (m ²)				4040.0	Property Line setback:	South	7.89
						West	0.90
	Zor	ning By-law 0225	-2007		Block B	Height:	9.50
FSI*				0.72		North	7.50
FSI**				0.63	Property Line setback:	East	13.70
Total GFA (m	²): Residential	I ZBL Definition	*	3642		South	4.50
Total GFA (m	r): Infill Reside	ential ZBL Defin	nition**	3210		West	0.90
*Calculated in	ncluding baser	ment but exclud	ing garage		Block C	Height:	9.50
**Calculated	excluding Bas	sement but inclu	ding garage			North	
					Property Line setback:	East	
				Property Line setback.	South		
						West	
					Block D	Height:	9.50
						North	
					Property Line setback:	East	
					1 Toperty Line Setback.	South	4.50

Paving	area area		Lo
Hard Landscape Area 232.0 4.58% of total site	area		Lo
Building Area (Combined Largest Footprints) 1357.0 26.81% of totalsite			
Building Heights & Seibacks (m) Height: 9,50 Detached Lot 1	area		Lo
Block A Height: 9,50 Detached Lot 1			Lo
Block A Height: 9,50 Detached Lot 1			В
North 4.50 East 12.02 Property Line setback: South 7.89 West 0.90			Lo
Property Line setback: South 7.89 Setback: South 7.89 Setback: South Setback: Setback:	Height:	9.00	Lo
South 7.89 setback: South 9.50 Detached Lot 1 South 9.50 South	North	2.44	Lo
South 7.89 setnack:	East	6.16	BI
Block B Height: 9.50 Detached Lot 1 North 7.50 Froperty Line setback: East 13.70 Property Line setback: South 4.50 setback:	South	2.40	В
North 7.50	West	8.37	Lo
Property Line setback: East 13.70 Property Line South 4.50 Property Line setback:	Height:	9.00	Lo
Property Line setback: South 4.50 setback:	North	2.40	Lo
South 4.50 setback:	East	6.16	BI
West 0.90	South	2.40	В
	West	8.37	Lo
Block C Height: 9.50 Detached Lot 1	Height:	9.00	Lo
North 4.50	North	2.40	Lo
East 0.90 Property Line	East	6.16	BI
Property Line setback: South 7.87 setback:	South	2.40	В
West 1.44	West	8.37	Lo
Block D Height: 9.50 Detached Lot 1	Height:	9.00	Lo
North 7.50	North	2.40	Lo
Property Line setback: East 0.90 Property Line	East	6.16	BI
South 4.50 setback:	South	2.40	1 🗏
West 1.87	West	8.37	C
Note: Building height measured from established grade.	*		. –

Calcula	esidential Area ations by Block and Lot Number	Gross Construction Area (m2)	Garage	Basement	Gross Floor Area (m2)*	Gross Floor Area (m2)**	Unit Mix Breakdown							
							1	1+Den	2	2+D€n	3	3+Den	4	4+De
	ed Homes													
Lot 1		341.0	38.0	89.0	303.0	252.0								1
Lot 2		341.0	38.0	89.0	303.0	252.0								1
Lot 3		341.0	38.0	89.0	303.0	252.0								1
Lot 4		341.0	38.0	89.0	303.0	252.0								1
Block A	4													
Lot 14	Unit Type 1	224.0	20.0	40.0	204.0	184.0				1				
Lot 15	Unit Type 1	219.0	19.0	39.0	200.0	180.0				1				
Lot 16	Unit Type 2	224.0	23.0	39.0	201.0	185.0				1				
Block A	Totals	667	62	118	605	549	0	0	0	3	0	0	0	0
Block E	3													
Lot 8	Unit Type 1	224.0	20.0	40.0	204.0	184.0				1				
Lot 9	Unit Type 1	219.0	19.0	39.0	200.0	180.0				1				
Lot 10	Unit Type 2	224.0	23.0	39.0	201.0	185.0				1				
Block B	Totals	667	62	118	605	549	0	0	0	3	0	0	0	0
Block C	3													
Lot 11	Unit Type 1	225.0	21.0	40.0	204.0	185.0				1				
Lot 12	Unit Type 1	221.0	20.0	39.0	201.0	182.0				1				
Lot 13	Unit Type 1	225.0	20.0	40.0	205.0	185.0				1				
Block C		671	61	119	610	552	0	0	0	3	0	0	0	0
Block D)													
Lot 5	Unit Type 1	225.0	21.0	40.0	204.0	185.0				1				
Lot 6	Unit Type 1	221.0	20.0	39.0	201.0	182.0				1				
Lot 7	Unit Type 1	225.0	20.0	40.0	205.0	185.0				1				
Block D		671	61	119	610	552	0	0	0	3	0	0	0	0
		110000		0.00				100	-					-

	Sheet List			
Sheet Number Sheet Name				
A000	Cover Page			
A001	Site Plan			
A002	Concept Plan			
A003	Typical Site Details			
A100	Basement			
A101	Level 1			
A102	Level 2			
A103	Level 3			
A104	Roof Plan			
A200	Block A/B Elevations			
A201	Block C/D Elevations			
A202	Detached Dwelling Elevations			





Project No:	1607
Scale:	As indicate
Date:	2017/04/0
Drawn by:	RV

Drawing Ti

Cover Page

Drawi Numb

A000



Block A	Garage	23 m²
Block A	Type 2	197 m²
Block A	Garage	19 m²
Block A	Type 1	200 m ²
Block A	Garage	20 m²
Block A	Type 1	204 m²
Block A: 15		663 m²

Block B	Garage	23 m²
Block B	Type 2	197 m²
Block B	Garage	19 m²
Block B	Type 1	200 m²
Block B	Garage	20 m²
Block B	Type 1	204 m²
Block B: 15		663 m²

Block C	Garage	20 m²
Block C	Type 1	205 m²
Block C	Garage	20 m²
Block C	Type 1	200 m²
Block C	Garage	21 m²
Block C	Type 1	205 m²
Block C: 15	•	671 m²

Block D	Garage	20 m²
Block D	Type 1	205 m²
Block D	Garage	20 m²
Block D	Type 1	200 m²
Block D	Garage	21 m²
Block D	Type 1	205 m²
Block D: 15	5	671 m²

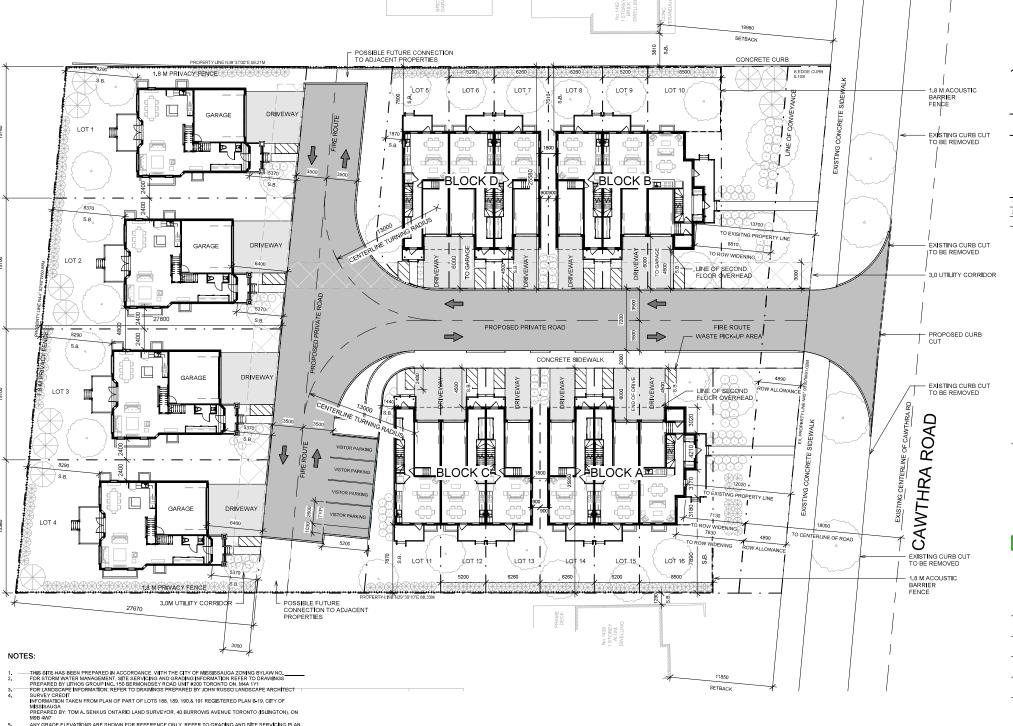
Detached 1	Basement	89 m²
Detached 1	Level 1	88 m²
Detached 1	Level 2	126 m²
Detached 1	Garage	38 m²
Datashad 4.	4	244 2

Detached 2		89 m²
Detached 2	Level 1	88 m²
Detached 2	Level 2	126 m²
Detached 2	Garage	38 m²
Detached 2:	4	341 m²

Detached 3	Basement	89 m²
Detached 3		88 m²
Detached 3	Level 2	126 m²
Detached 3	Garage	38 m²
Detached 3:	Λ	3/11 m²

Detached 4	Basement	89 m²
Detached 4	Level 1	88 m²
Detached 4	Level 2	126 m²
Detached 4	Garage	38 m²
Detached 4:	4	341 m²

Ar	ea Sch	edule 1	otal	
			4032	m²



1444 1458

1444-1458 CAWTHRA ROAD MISSISSAUGA, ON

© Copyright KFA Architects and Planners Inc., all rights reserved. No part of this document whether printed form or supplied as digital data may be reproduced, stored in a retirved system or supplied to the property of the property of the property of the photocopyring, recording or otherwise without the prior written permission of KFA Architects and Pfanners (ps. All dimensions to be checked on site by the contractor, Drawings are not to be scaled, and any discrepancies are to be reported to the Architect to the property of the property of the property of the Architect of the property of the property of the Architect of the property of the property of the property of the Architect of the property of the property of the property of the Architect of the property of the property of the property of the Architect of the property of the proper

1	Issue to Consultants	2018.09.12
2	Issue for OP/RZ	2018.09.28



Project No:	1607
Scale:	As indicate
Date:	2017/04/0
Drawn by:	R,V,W
Drawing Title	

Site Plan

Drawing Number

A001

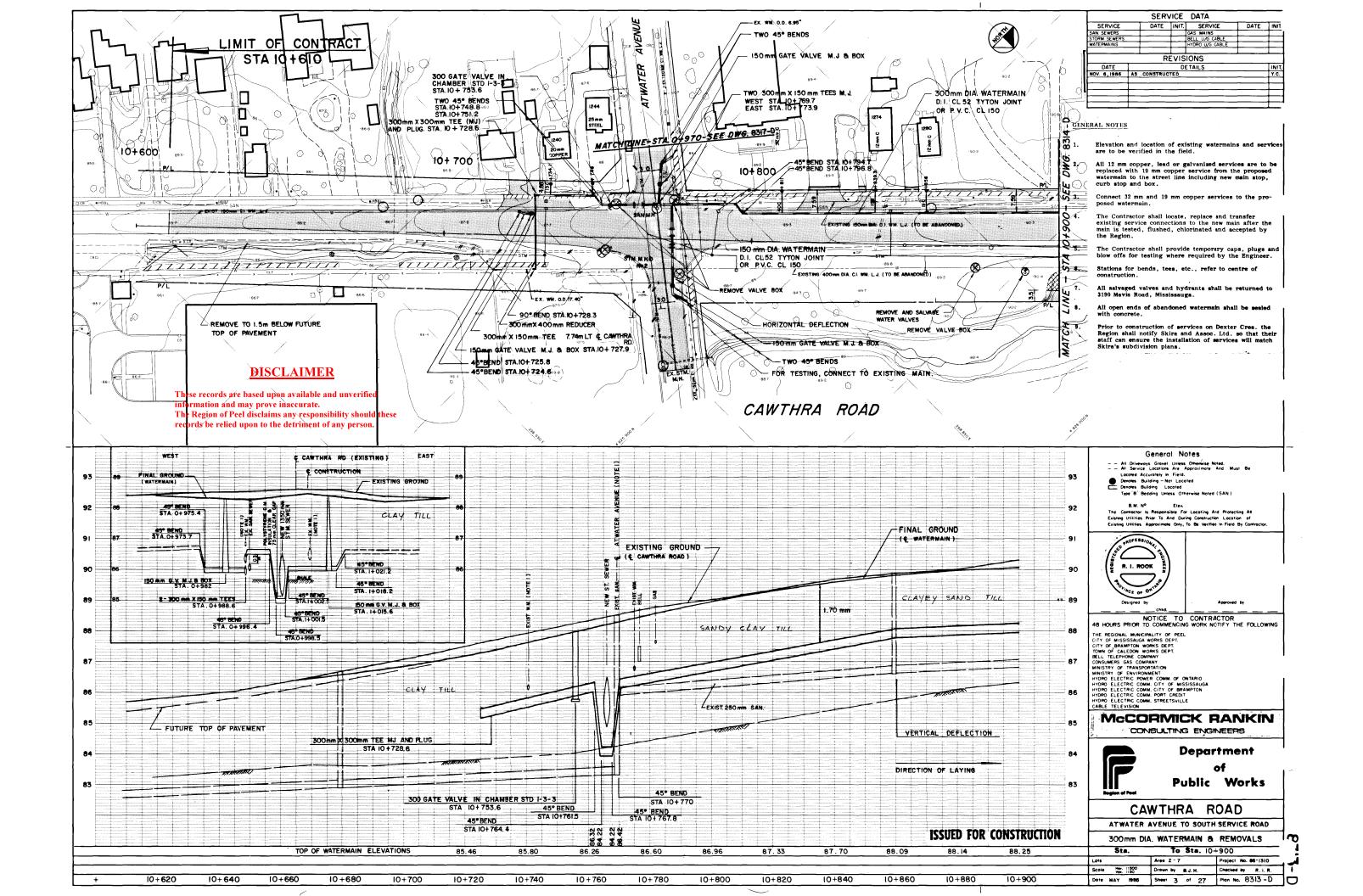
MOS AVY

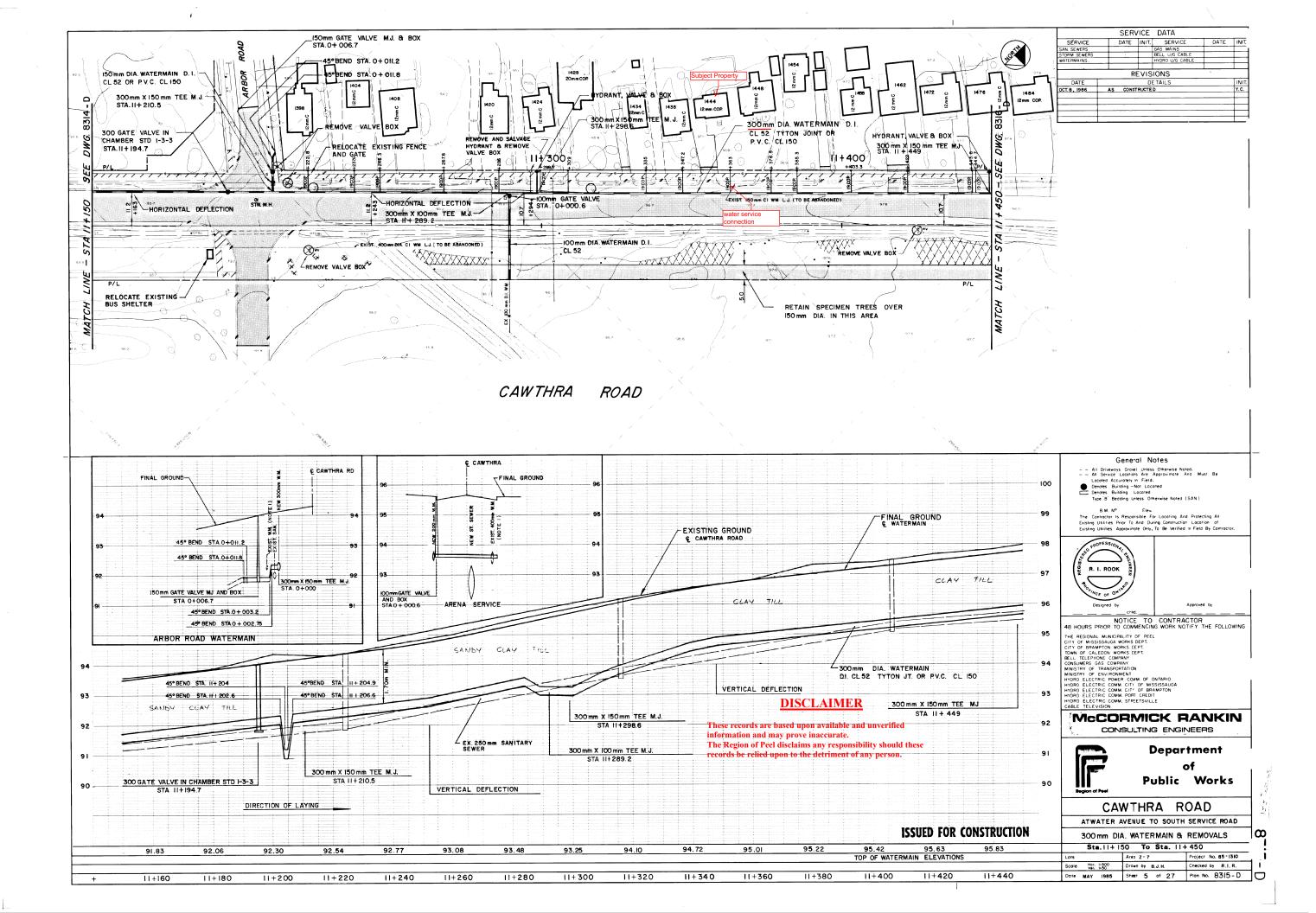
ANY ORADE ELEVATIONS ARE SHOWN FOR REFERENCE ONLY, REFER TO GRADING AND SITE SERVICING PLAN
FOR GRADING AND UIG SERVICES

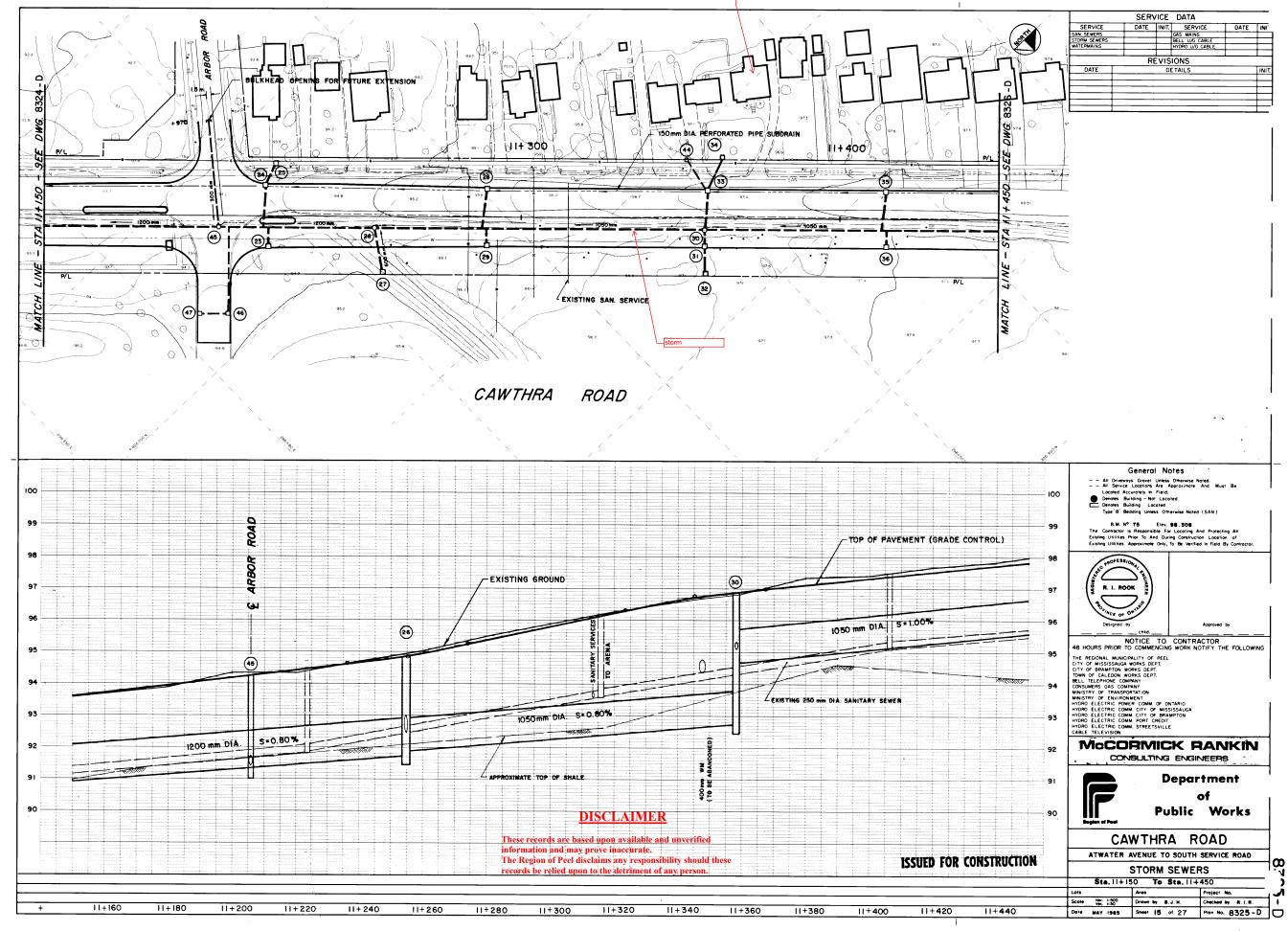
ALL SITE AREA LISHING TO BE DIRECTED DOWNWARD AND DEFECTED AWAY FROM ADJACENT LOTS ROADS
AND STREETS

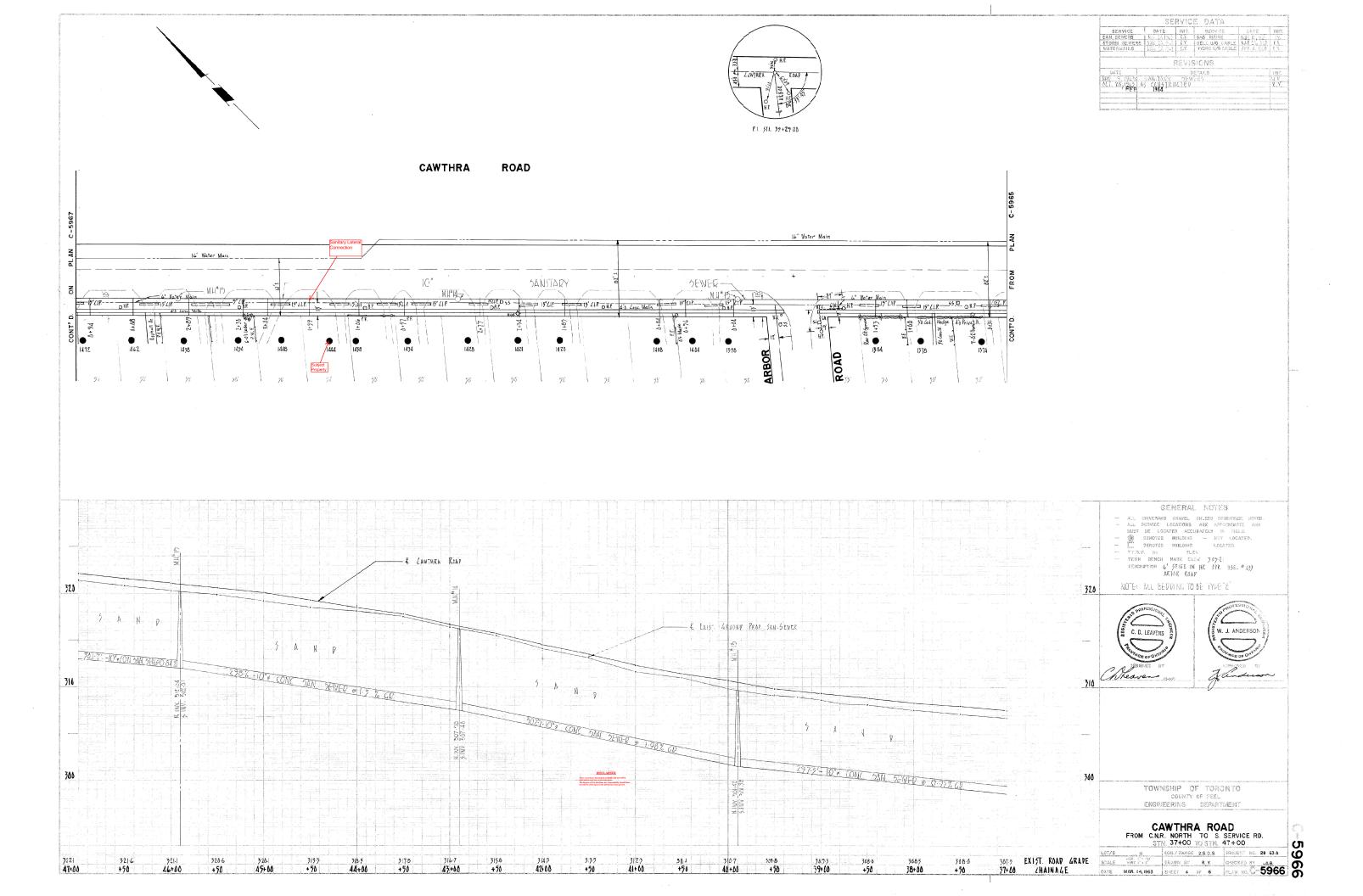
ALL CURBING AND DRIVEWAY ENTRANCES TO BE DESIGNED IN ACCORDANCE WITH THE CITY'S MATERIALS
STANDARDS AND SPECIFICATIONS MANUAL
OF STANDARDS AND TO THE SATISFACTION OF THE
CHEF ENGINEER, EXECUTIVE DIRECTOR OF ENDINEERING AND CONSTRUCTION SERVICES
OF STANDARDS AND SPECIFICATION OF THE CHEF ENDINEER, EXECUTIVE DIRECTOR OF ENDINEERING AND CONSTRUCTION SERVICES

SITE SERVICES DISCLAMER
OF AND SPECIFICATION OF STANDARDS AND TO THE SATISFACTION OF THE
THAN ONE CONDOMINIUM CORPORATION ENCOMPASSING ANY OR ALL OF THIS DEVELOPMENT OR MAKE AN APPLICATION
THAT RESULTS IN A LAND DIMENSION, STAFF MAY REQUIRE LEGAL ASSURANCES WILL BE DETERMINED AT THE TIME OF
THE APPLICATION FOR CONDOMINUM APPROVACL.

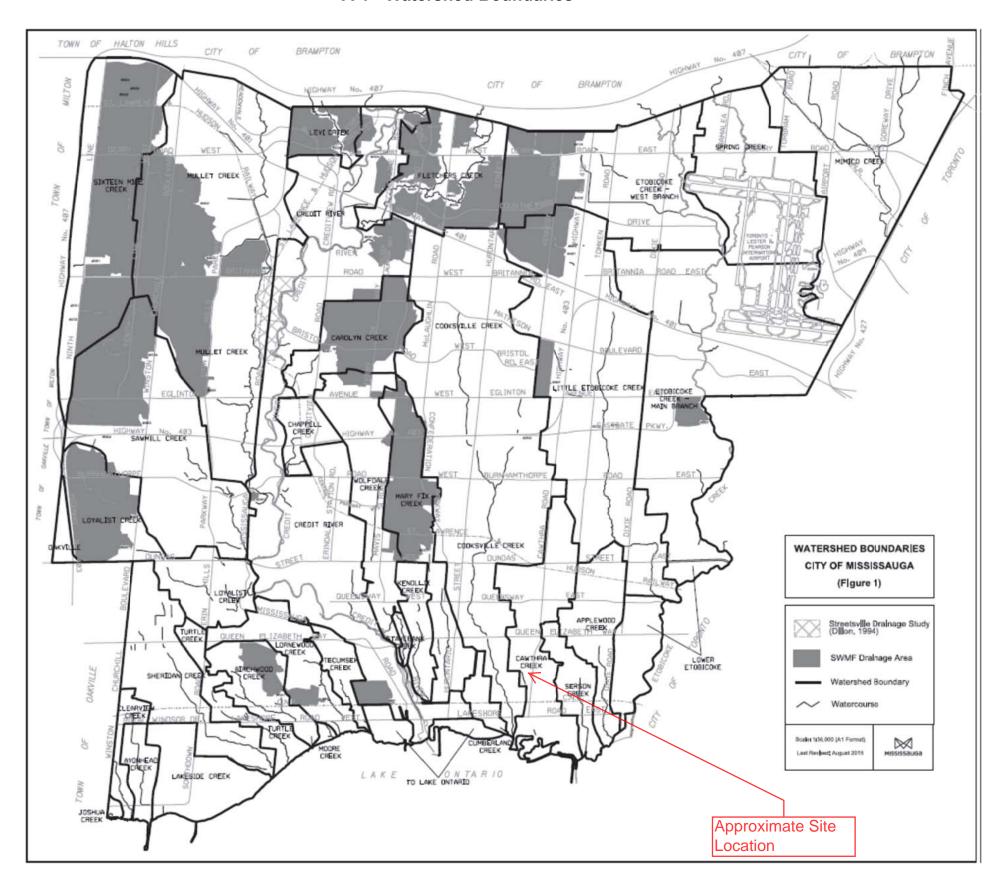




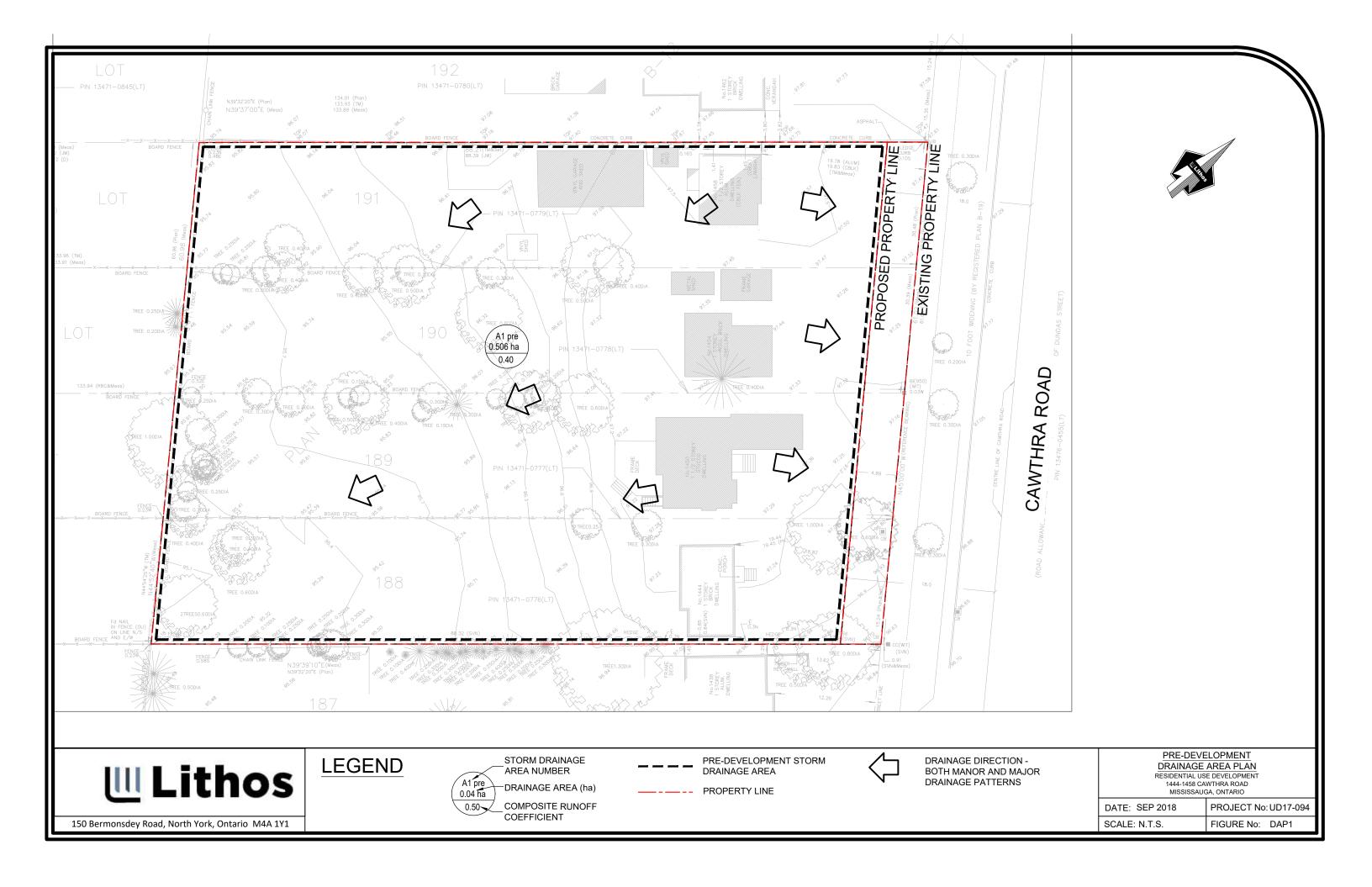




A-1 - Watershed Boundaries



APPENDIX C Storm Analysis





Rational Method

Pre-Development Flow Calculation

1444-1458 Cawthra Road File No. UD17-094

> City of Mississauga Date: September 2018

Prepared by: Angelos Andreadis, P.E., M.A.Sc. Reviewed by: Nick Moutzouris, P.Eng., M.A.Sc.

Input Parameters

 Area Number
 Area
 C
 Tc

 (ha)
 (min.)

 A1 pre
 0.506
 0.40
 15

Q = 0.0028 C I A

Rational Method Calculation

Event 2 yr

IDF Data Set City of Missisauga

a = 610 b = 4.6 c = 0.78

Area Number	Α	С	AC	Tc	I	Q	Q
	(ha)			(min.)	(mm/h)	(m³/s)	(L/s)
A1 pre	0.506	0.40	0.20	15	59.9	0.034	33.7

Event 5 yr

IDF Data Set City of Missisauga

a = 820 b = 4.6 c = 0.78

Area Number	Α	С	AC	Тс	ı	Q	Q
	(ha)			(min.)	(mm/h)	(m³/s)	(L/s)
A1 pre	0.506	0.40	0.20	15	80.5	0.045	45.3

Event 10 yr

IDF Data Set City of Missisauga

a = 1010 b = 4.6 c = 0.78

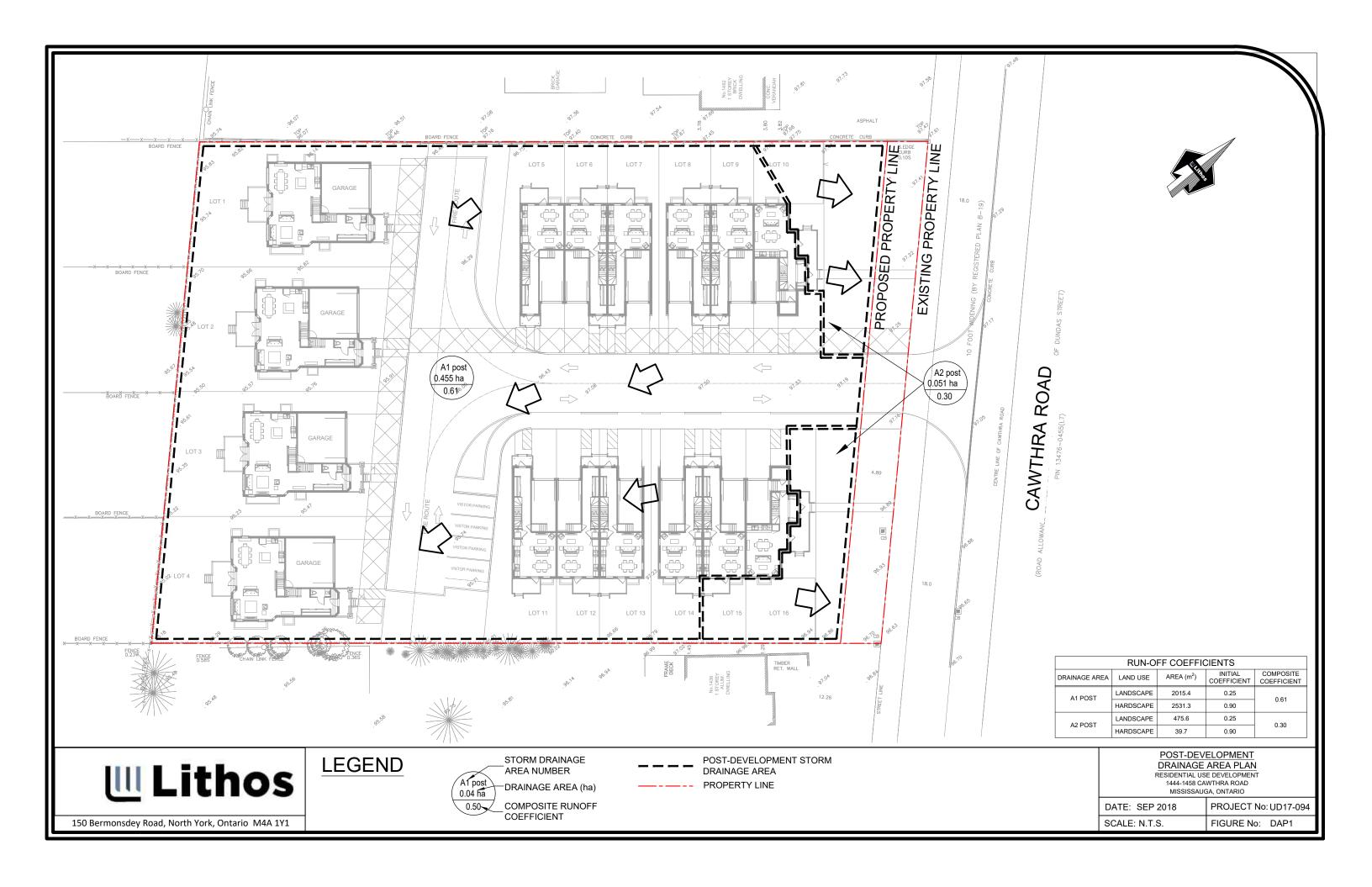
Area Number	Α	С	AC	Tc	I	Q	Q
	(ha)			(min.)	(mm/h)	(m³/s)	(L/s)
Area Number	0.506	0.40	0.20	15	99.2	0.056	55.8

Event 100 yr

IDF Data Set City of Missisauga

a = 1450 b = 4.9 c = 0.78

Area Number	Α	С	AC	Tc	I	Q	Q
	(ha)			(min.)	(mm/h)	(m³/s)	(L/s)
A1 pre	0.506	0.40	0.20	15	140.7	0.079	79.1





Modified Rational Method - Two Year Storm Site Flow and Storage Summary 1444-1458 Cawthra Road File No. UD17-094 Date: September 2018

Prepared By: Angelos Andreadis, P.Eng.,M.A.Sc. Reviewed By: Nick Moutzouris, P.Eng., M.A.Sc.

Reviewed By: Nic	ck Moutzouris, P.En	g., м.А.Sc.						
		Controlled - A1 Post				Drainage Area A2 Post Uncontrolled		
		Drainage Areas	A1 Post			one on a contraction of		
		Area (A1) =	0.455	ha		Area (A2) =	0.051	ha
		"C" =	0.61			"C" =	0.30	
		AC1=	0.28			AC2=	0.02	
		Tc =	15.0	min		Tc =	15.0	min
		Time Increment =	5.0	min				
						Max. Release Rate =	2.6	L/s
		Controlled Release Rate =	26.2	L/s				
		Min. Storage =	18.1	m ³				
2-Year De	esign Storm	Will Storago	10.1					
a=	610.00	Type	Area (ha)	"C"	1	Type	Area (ha)	"C"
b=	4.60	Landscaped	0.202	0.25	1	Landscaped	0.048	0.25
c=	0.78	Hardscaped	0.253	0.90	1	Hardscaped	0.004	0.90
1=	a (b + t) ^c	Total Area (A1)	0.455	0.61	1	Total Area (A2)	0.051	0.30
	u (5 · t)			1	4			3.50
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	
, ,		Storm	Runoff	Target	Total	Storm	Runoff	
Time	Rainfall	Storiii	Kulloli	Released	Required	Storm		
	Intensity	Runoff	Volume	Volume	Storage	Runoff	Volume	
	intensity	(A1 post)	(A1 post)	(A1 post)	(A1 post)	(A2 post)	(A2 Post)	
(min)	(mm/hr)	(m³/s)	(m³)	(m³)	(m³)	(m³/s)	(m ³)	
15.0	59.9	0.046	41.66	23.55	18.11	0.003	2.31	
20.0	50.2	0.039	46.52	31.40	15.12	0.002	2.58	
25.0	43.4	0.034	50.34	39.25	11.09	0.002	2.79	
30.0	38.4	0.030	53.48	47.09	6.38	0.002	2.96	
35.0	34.6	0.027	56.16	54.94	1.21	0.001	3.11	
40.0	31.5	0.024	58.49	62.79	0.00	0.001	3.24	
45.0	29.0	0.022	60.57	70.64	0.00	0.001	3.35	
50.0	26.9	0.021	62.45	78.49	0.00	0.001	3.46	
55.0	25.2	0.019	64.15	86.34	0.00	0.001	3.55	
60.0	23.6	0.018	65.72	94.19	0.00	0.001	3.64	
65.0	22.3	0.017	67.18	102.04	0.00	0.001	3.72	
70.0	21.1	0.016	68.53	109.89	0.00	0.001	3.79	
75.0	20.1	0.016	69.81	117.74	0.00	0.001	3.86	
80.0	19.1	0.015	71.00	125.59	0.00	0.001	3.93	
85.0	18.3	0.014	72.14	133.43	0.00	0.001	3.99	
90.0	17.5	0.014	73.21	141.28	0.00	0.001	4.05	
95.0	16.9	0.013	74.24	149.13	0.00	0.001	4.11	
100.0	16.2	0.013	75.21	156.98	0.00	0.001	4.16	
105.0	15.6	0.012	76.15	164.83	0.00	0.001	4.22	
110.0	15.1	0.012	77.05	172.68	0.00	0.001	4.27	
115.0	14.6	0.011	77.91	180.53	0.00	0.001	4.31	
120.0	14.2	0.011	78.74	188.38	0.00	0.001	4.36	
125.0	13.7	0.011	79.55	196.23	0.00	0.001	4.40	
130.0	13.3	0.010	80.32	204.08	0.00	0.001	4.45	
135.0	13.0	0.010	81.07	211.93	0.00	0.001	4.49	
140.0	12.6	0.010	81.80	219.78	0.00	0.001	4.53	
145.0	12.3	0.009	82.50	227.62	0.00	0.001	4.57	
150.0	12.0	0.009	83.19 83.85	235.47	0.00 0.00	0.001 0.000	4.60 4.64	
155.0	11.7	0.009		243.32			4.64 4.68	
160.0 165.0	11.4 11.1	0.009 0.009	84.50	251.17 259.02	0.00 0.00	0.000 0.000	4.68 4.71	
	11.1 10.9	0.009	85.13 95.74				4.71 4.75	
170.0	10.9	υ.υυδ	85.74	266.87	0.00	0.000	4./0	



Modified Rational Method - Five Year Storm Site Flow and Storage Summary 1444-1458 Cawthra Road File No. UD17-094 Date: September 2018

Prepared By: Angelos Andreadis, P.Eng.,M.A.Sc. Reviewed By: Nick Moutzouris, P.Eng., M.A.Sc.

Reviewed By: Nic	ck Moutzouris, P.En	g., M.A.Sc.						
		Controlled - A1 Post				Drainage Area A2 Post Uncontrolled		
		Drainage Areas	A1 Post			Gricoria Glica		
		Area (A1) =	0.455	ha		Area (A2) =	0.051	ha
		"C" =	0.61			"C" =	0.30	
		AC1=	0.28			AC2=	0.02	
		Tc=	15.0	min		Tc =	15.0	min
		Time Increment =	5.0	min			15.0	1111111
		Time increment -	5.0	111111		Max. Release Rate =	3.4	L/s
		On the Head Balance Bate -	00.0	1.7-		iviax. Release Rate –	3.4	L/S
		Controlled Release Rate =	26.2	L/s				
		Min. Storage =	32.4	m ³				
5-Year De	esign Storm				-			
a=	820.00	Туре	Area (ha)	"C"	_	Туре	Area (ha)	"C"
b=	4.60	Landscaped	0.202	0.25	_	Landscaped	0.048	0.25
C=	0.78	Hardscaped	0.253	0.90	_	Hardscaped	0.004	0.90
1 =	a (b + t) ^c	Total Area (A1)	0.455	0.61		Total Area (A2)	0.051	0.30
				•	-			
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	
		Storm	Runoff	Target	Total	Storm	Runoff	
Time	Rainfall			Released	Required			
	Intensity	Runoff	Volume	Volume	Storage	Runoff	Volume	
	intolloity	(A1 post)	(A1 post)	(A1 post)	(A1 post)	(A2 post)	(A2 Post)	
(min)	(mm/hr)	(m³/s)	(m³)	(m³)	(m³)	(m³/s)	(m³)	
15.0	80.5	0.062	56.00	23.55	32.45	0.003	3.10	
20.0	67.4	0.052	62.54	31.40	31.14	0.003	3.46	
25.0	58.4	0.045	67.66	39.25	28.42	0.002	3.75	
30.0	51.7	0.040	71.89	47.09	24.79	0.002	3.98	
35.0	46.5	0.036	75.49	54.94	20.55	0.002	4.18	
40.0	42.4	0.033	78.63	62.79	15.84	0.002	4.35	
45.0	39.0	0.030	81.43	70.64	10.78	0.002	4.51	
50.0	36.2	0.028	83.94	78.49	5.45	0.002	4.65	
55.0	33.8	0.026	86.24	86.34	0.00	0.001	4.77	
60.0	31.8	0.025	88.35	94.19	0.00	0.001	4.89	
65.0	30.0	0.023	90.30	102.04	0.00	0.001	5.00	
70.0	28.4	0.022	92.13	109.89	0.00	0.001	5.10	
75.0	27.0	0.021	93.84	117.74	0.00	0.001	5.19	
0.08	25.7	0.020	95.45	125.59	0.00	0.001	5.28	
85.0	24.6	0.019	96.97	133.43	0.00	0.001	5.37	
90.0	23.6	0.018	98.42	141.28	0.00	0.001	5.45	
95.0	22.7	0.018	99.79	149.13	0.00	0.001	5.52	
100.0	21.8	0.017	101.11	156.98	0.00	0.001	5.60	
105.0	21.0	0.016	102.37	164.83	0.00	0.001	5.67	
110.0	20.3	0.016	103.57	172.68	0.00	0.001	5.73	
115.0	19.6	0.015	104.73	180.53	0.00	0.001	5.80	
120.0	19.0	0.015	105.85	188.38	0.00	0.001	5.86	
125.0	18.4	0.014	106.93	196.23	0.00	0.001	5.92	
130.0	17.9	0.014	107.97	204.08	0.00	0.001	5.98	
135.0	17.4	0.013	108.98	211.93	0.00	0.001	6.03	
140.0	16.9	0.013	109.96	219.78	0.00	0.001	6.09	
145.0	16.5	0.013	110.90	227.62	0.00	0.001	6.14	
150.0	16.1	0.012	111.82	235.47	0.00	0.001	6.19	
155.0	15.7	0.012	112.72	243.32	0.00	0.001	6.24	
160.0	15.3	0.012	113.59	251.17	0.00	0.001	6.29	
165.0	15.0	0.012	114.43	259.02	0.00	0.001	6.33	
170.0	14.6	0.011	115.26	266.87	0.00	0.001	6.38	



Modified Rational Method - Ten Year Storm Site Flow and Storage Summary 1444-1458 Cawthra Road File No. UD17-094 Date: September 2018

PreparedBy:AngelosAndreadis,P.Eng.,M.A.Sc. Reviewed By: Nick Moutzouris, P.Eng., M.A.Sc.

•	ck Moutzouris, P.Eng							
		Controlled - A1 Post				Drainage Area A2 Post Uncontrolled		
		Drainage Areas	A1 Post					
		Area (A1) =	0.455	ha		Area (A2) =	0.051	ha
		"C" =	0.61			"C" =	0.30	
		AC1=	0.28			AC2=	0.02	
		Tc =	15.0	min		Tc =	15.0	min
		Time Increment =	5.0	min		Max. Release Rate =	4.2	L/s
		Controlled Release Rate =	26.2	L/s		Wax. Nelease Nate -	4.2	L/3
		Min. Storage =	45.6	m ³				
10-Year D	esign Storm 1010.00	Turno	Area (ha)	"C"	1	Type	Aroa (ba)	"C"
	4.60	Type	0.202	0.25	4		Area (ha) 0.048	0.25
b=	0.78	Landscaped			-	Landscaped	0.048	
c=		Hardscaped	0.253	0.90	1	Hardscaped		0.90
1=	a (b + t) ^c	Total Area (A1)	0.455	0.61	1	Total Area (A2)	0.051	0.30
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	
Time	Rainfall	Storm	Runoff	Target Released	Total Required	Storm	Runoff	
10		Runoff	Volume	Volume	Storage	Runoff	Volume	
	Intensity	(A1 post)	(A1 post)	(A1 post)	(A1 post)	(A2 post)	(A2 Post)	
(min)	(mm/hr)	(m³/s)	(m³)	(m³)	(m³)	(m³/s)	(m ³)	
15.0	99.2	0.077	68.97	23.55	45.42	0.004	3.82	
20.0	83.1	0.064	77.02	31.40	45.63	0.004	4.26	
25.0	71.9	0.056	83.34	39.25	44.10	0.003	4.61	
30.0	63.7	0.049	88.55	47.09	41.45	0.003	4.90	
35.0	57.3	0.044	92.98	54.94	38.04	0.002	5.15	
40.0	52.2	0.040	96.85	62.79	34.06	0.002	5.36	
45.0	48.1	0.037	100.29	70.64	29.65	0.002	5.55	
50.0	44.6	0.034	103.39	78.49	24.90	0.002	5.72	
55.0	41.7	0.032	106.22	86.34	19.88	0.002	5.88	
60.0	39.1	0.030	108.82	94.19	14.63	0.002	6.02	
65.0	36.9	0.029	111.23	102.04	9.19	0.002	6.16	
70.0	35.0	0.027	113.47	109.89	3.59	0.001	6.28	
75.0	33.2	0.026	115.58	117.74	0.00	0.001	6.40	
80.0	31.7	0.024	117.56	125.59	0.00	0.001	6.51	
85.0	30.3	0.023	119.44	133.43	0.00	0.001	6.61	
90.0	29.0	0.022	121.22	141.28	0.00	0.001	6.71	
95.0	27.9	0.022	122.92	149.13	0.00	0.001	6.80	
100.0	26.9	0.021	124.54	156.98	0.00	0.001	6.89	
105.0	25.9	0.020	126.09	164.83	0.00	0.001	6.98	
110.0	25.0	0.019	127.57	172.68	0.00	0.001	7.06	
115.0	24.2	0.019	129.00	180.53	0.00	0.001	7.14	
120.0	23.4	0.018	130.38	188.38	0.00	0.001	7.22	
125.0	22.7	0.018	131.71	196.23	0.00	0.001	7.29	
130.0	22.1	0.017	132.99	204.08	0.00	0.001	7.36	
135.0	21.4	0.017	134.23	211.93	0.00	0.001	7.43	
140.0	20.9	0.016	135.43	219.78	0.00	0.001	7.50	
145.0	20.3	0.016	136.60	227.62	0.00	0.001	7.56	
150.0	19.8	0.015	137.73	235.47	0.00	0.001	7.62	
155.0	19.3	0.015	138.83	243.32	0.00	0.001	7.69	
160.0	18.9	0.015	139.91	251.17	0.00	0.001	7.74	
165.0	18.4	0.014	140.95	259.02	0.00	0.001	7.80	
170.0	18.0	0.014	141.97	266.87	0.00	0.001	7.86	



Modified Rational Method - Hundred Year Storm Site Flow and Storage Summary 1444-1458 Cawthra Road File No. UD17-094 Date: September 2018

Prepared By: Angelos Andreadis, P.E Reviewed By: Nick Moutzouris, P.Eng., M.A.Sc.

reviewed By: Nic	ck Moutzouris, P.En	y., IVI.A.SC.				T		
		Controlled - A1 Post				Drainage Area A2 Post Uncontrolled		
		Drainage Areas Area (A1) = "C" = AC1=	A1 Post 0.455 0.76 0.35	ha		Area (A2) = "C" = AC2=	0.051 0.37 0.02	ha
Adiustm	nent Factor	Tc =	15.0	min		Tc =	15.0	min
) =1.25 *C	Time Increment =	5.0	min		16 -	10.0	
0(100)	7 1.20 0	Time increment	0.0			Max. Release Rate =	7.5	L/s
		Controlled Release Rate =	26.2	L/s		Max. Holodoo Hato		2,0
		Min. Storage =	110.9	m ³				
100-Year [Design Storm	Wiiii. Otorage =	110.5					
a=	1450.00	Type	Area (ha)	"C"	7	Type	Area (ha)	"C"
b=	4.90	Landscaped	0.202	0.25	┪	Landscaped	0.048	0.25
C=	0.78	Hardscaped	0.253	0.90	1	Hardscaped	0.004	0.90
I =	a (b + t) ^c	Total Area (A1)	0.455	0.61	┪	Total Area (A2)	0.051	0.30
! =	a (D + t)	Total Alea (A1)	0.433	0.01		Total Alea (A2)	0.031	0.50
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	
Time	Rainfall	Storm	Runoff	Target Released	Total Required	Storm	Runoff	
	Intensity	Runoff (A1 post)	Volume (A1 post)	Volume (A1 post)	Storage (A1 post)	Runoff (A2 post)	Volume (A2 Post)	
(min)	(mm/hr)	(m³/s)	(m ³)	(m ³)	(m ³)	(m³/s)	(m ³)	
15.0	140.7	0.136	122.31	23.55	98.77	0.008	6.77	
20.0	118.1	0.114	136.92	31.40	105.53	0.006	7.58	
25.0	102.4	0.099	148.39	39.25	109.14	0.005	8.21	
30.0	90.8	0.088	157.84	47.09	110.74	0.005	8.74	
35.0	81.8	0.079	165.88	54.94	110.94	0.004	9.18	
40.0	74.6	0.072	172.90	62.79	110.11	0.004	9.57	
45.0	68.7	0.066	179.14	70.64	108.49	0.004	9.92	
50.0	63.8	0.062	184.75	78.49	106.26	0.003	10.23	
55.0	59.6	0.058	189.87	86.34	103.53	0.003	10.51	
60.0 65.0	56.0 52.8	0.054 0.051	194.58 198.93	94.19 102.04	100.39 96.90	0.003 0.003	10.77 11.01	
70.0	52.6 50.0	0.031	203.00	102.04	93.11	0.003	11.24	
75.0	47.6	0.048	206.81	117.74	89.07	0.003	11.45	
80.0	45.4	0.044	210.39	125.59	84.81	0.002	11.65	
85.0	43.4	0.042	213.78	133.43	80.35	0.002	11.83	
90.0	41.6	0.040	217.00	141.28	75.72	0.002	12.01	
95.0	40.0	0.039	220.06	149.13	70.93	0.002	12.18	
100.0	38.5	0.037	222.99	156.98	66.01	0.002	12.34	
105.0	37.1	0.036	225.79	164.83	60.96	0.002	12.50	
110.0	35.8	0.035	228.47	172.68	55.79	0.002	12.65	
115.0	34.7	0.033	231.05	180.53	50.52	0.002	12.79	
120.0	33.6	0.032	233.53	188.38	45.16	0.002	12.93	
125.0 130.0	32.6 31.6	0.031 0.031	235.93 238.24	196.23 204.08	39.70 34.17	0.002 0.002	13.06 13.19	
135.0	30.7	0.031	240.48	211.93	28.56	0.002	13.19	
140.0	29.9	0.030	242.65	219.78	22.88	0.002	13.43	
145.0	29.1	0.028	244.75	227.62	17.13	0.002	13.55	
150.0	28.4	0.027	246.80	235.47	11.32	0.002	13.66	
155.0	27.7	0.027	248.78	243.32	5.46	0.001	13.77	
160.0	27.0	0.026	250.71	251.17	0.00	0.001	13.88	
165.0	26.4	0.026	252.59	259.02	0.00	0.001	13.98	
170.0	25.8	0.025	254.43	266.87	0.00	0.001	14.08	

APPENDIX D Sanitary Data Analysis



SANITARY SEWER DESIGN SHEET

1444-1458 Cawthra Road CITY OF MISSISSAUGA

		RESIDENTIAL						COMME	COMMERCIAL FLOW SEWER I									DESIGN					
																			SEWER DESIGN				
LOCATION	SECTION AREA	Single Family (<10m frontage)	Single Family (>10m frontage)	Semi- Detached	Row Dwellings	Apartments	Apartments >475p/ha	SECTION POP.	COMMERCIAL AREA	SECTION POP. @ 50p/ha	TOTAL ACCUM. POP.	AVERAGE RESIDENTIAL FLOW '@' 302.8 L/c/d	HARMON PEAKING FACTOR	RES. PEAK FLOW	AVERAGE COMMERCIAL FLOW @ 302.8 L/c/d	TOTAL ACCUM. AREA	0.2 L/s/ha.	TOTAL DESIGN FLOW	PIPE LENGTH	PIPE DIA.	SLOPE	FULL FLOW CAPACITY n = 0.013	% of DESIG CAPACITY
	(ha.)	@ 70p/ha	@ 50p/ha	@ 70p/ha	@ 175p/ha	@ 475p/ha	@ 2.7 ppu	(persons)	(ha.)	(persons)	(persons)	(L/s)		(L/s)	(L/s)	(ha.)	(L/s)	(L/s)	(m)	(mm)	(%)	(L/sec)	(%)
column number	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23
Existing Condition																							
Residential Dwellings	0.536	0.00	0.042	0.00	0.00	0.00	0.00	2	0.00	0	2	0.007	4.46	0.033	0.00	0.536	0.107	0.14					
Proposed Condition																							
Residential-Use Development	0.536	0.00	0.121	0.00	0.243	0.00	0.00	49	0.00	0	49	0.170	4.32	0.735	0.00	0.536	0.107	0.84					
Note: Worst case scenario discharate been accounted to determine the to Residential/Commercial Flow Rainfiltration - 0.2 L/ha Peaking Factor = 1 + [14 / (4 + PSite Area: 0.536 ha	otal net flow	due to the pro	posed develop y													Total N	let Flow	0.70					
ய Litho	S		Prepared b Reviewed I Date: Sept	y: Nick I	Moutzouri						Project I	1444-1458 No: UD17-09 ississauga		Road	•						ı	Sheet 1 (DF 1

APPENDIX E Water Data Analysis



WATER DEMAND

1444-1458 Cawthra Road

File No: PUD17-094
Date: September 2018

Prepared by: Angelos Andreadis, P.E., M.A.Sc. Reviewed By: Nick Moutzouris, P.Eng., M.A.Sc.

Note: The levels indicated, reference the worst

case scenario for townhouse fire separation

according to the OBC

Fire Flow Calculation

1 F= 220 C (A)^{1/2}

Where F= Fire flow in Lpm

C= construction type coefficient

= 1.0 Ordinary Construction

A = total floor area in sq.m. excluding basements, includes garage*

Area Applied

= 300 sq.m.

F = 3,810.51 L/min

F = 3,800 L/min Round to nearest 100 l/min

2 Occupancy Reduction

25% non-combustible occupancy F = 2850 L/min

3 Sprinkler Reduction

0% Reduction for NFPA Sprinkler System

F = 2850 I/min

4 Separation Charge

 15% N
 10.1 to 20m

 25% E
 0 to 3m

 25% W
 0 to 3m

 10% S
 20.1 to 30m

75% Total Separation Charge

F = 4,988.00 L/min 83.13 L/s F = 1318 US GPM

Domestic Flow Calculations

Population = 44 Persons (from sanitary design sheet for Residential)
Commercial Area = 0 Persons (from sanitary design sheet for Commercial)

Average Day Demand = 280 L/cap/day 1 US Gallon=3.785 L

2138 L/min

= = 0.14 L/s

= 2 US GPM 1 US GPM=15.852L/s

Max. Daily Demand Peaking Factor = 2.0 (For residential)

Max. Daily Demand = 0.29 L/s = 5 US GPM

Max. Hourly Demand Peaking Factor = 3.0

Max. Hourly Demand = 0.43 L/s = 7 US GPM

Max Daily Demand = 0.29 L/s Fire Flow = 83.13 L/s

Required 'Design' Flow = 83.42 L/s Note: Required 'Design' Flow is the maximum of either:

1322 US GPM 1) Fire Flow + Maximum Daily Demand

2) Maximum Hourly Demand



WATER DEMAND

1444-1458 Cawthra Road

File No: PUD17-094 Date: September 2018

Prepared by: Angelos Andreadis, P.E., M.A.Sc. Reviewed By: Nick Moutzouris, P.Eng., M.A.Sc.

22.47 psi (20.3+Hf)

Pressure Losses

Hazen-Williams Formula

 $V = kCR_h^{0.63}xS^{0.54}$

k= 0.85 - conversion factor (0.849 for SI units and 1.318 for US customary units)

C= 140 - roughness coefficient (PVC: 140-150)

S= h_f/L

Rh= D/4 - hydraulic radius (D/4 for full flow, A/P_W for partially flow)

Fire Fighting and Domestic Head Loss

L/s	83.4	Flow Requirements=
mm	150	Diameter=
m^2	1.77E-02	Area=
m	13	L=
m/s	4.72	V=
	1.17E-01	S=
	0.04	R _h =
m	1.52	H _f =
psi	2.17	=

Flow Test (dated: April 11, 2018)

when:	Static Pressure =	64 psi	Flow =	0	GPM	=	0.00 L/s
F	Residual Pressure =	58 psi	Flow =	1950	GPM	=	123.01 L/s

Pressure

59.9

Based on the Pressure/Flow relationship, we have to confirm that the flow requirement of (psi) Flow (L/s) 83.42 L/s can be provided at minimum pressure (20.3 psi + Losses) as set out by the FUS 0.00 123.01 guidelines 58

83.42

Fire Flow is above minimum of

Since the flow of 83.42 L/s required for the proposed development is provided in the existing watermain at 59.9 psi (which is more than the minimum

of 22.47 psi), we anticipate that the existing watermain infrastructure can support the proposed development.

HYDRANT FLOW TEST FORM			COLE ENGINEERING						
Project No: 2018 -	-0046	Date:	Apr. 11, 2018						
	& Causthra Rd. Hyd								
Uississo	uga, Dr.	Tested By:	Coolen X Samouthan						
1) Required photos:									
Site Id & Date	Site Id & Date Condition of Flow Hydrant								
Location Overview	Condition of Resid	ual Hydrant							
Other									
2) Test Data									
Time of Test: 1300									
Location of Test: (Flow)	+ of 1424 Ca	wthra los,	south side						
Location of Test: (Flow) (Residual) (Residual)	4 / 1476 Can	wthra Rd. S	outh side						
Main Size: 300 mm	V	,	1						
Static Pressure: 64 psi									
Number of Outlets & Orifice Size	Pitot Pressure	Flow (USGPM)	Residual Pressure						
1 × 25"	54	1250	60						
2 × 2-5 ^a	34	1950	58						
4									
3) Calculations Q= 29.83 cd ² Vp		Where c- cofficient o	of discharge (1 in smooth pipe)						
Q1 = (29.83)(0.9)(2.5")2754	d- pipe diame p- pitot readir	eter (inches)						
= 1233.03 Q- flow (USGPM)									
Q1 = ~ 1250 USGPM									
ar = 2 (29.83)(0.9)(2.5")2 / 34									
= 1956.79									
Q+ = ~ 1950 USUPM		2							
Note: Hydrants tested accor			d Practice for Fire Flow						
10	esting and Markin	g of Hydrants							

