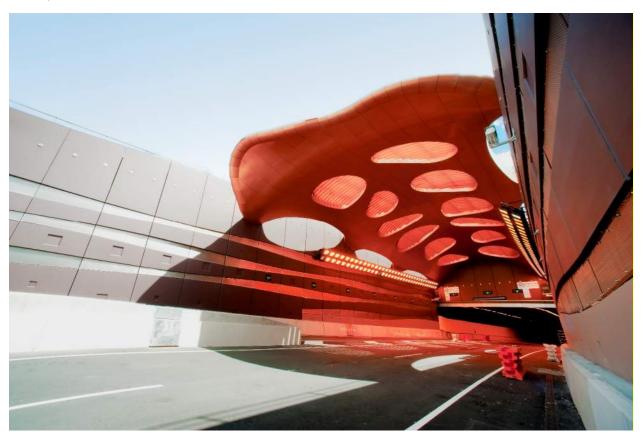
#### **EDENSHAW ANN DEVELOPMENTS LIMITED**

# 22-28 ANN STREET & 78 PARK STREET EAST

### **FUNCTIONAL SERVICING REPORT**

MAY 10, 2019







# 22-28 ANN STREET & 78 PARK STREET EAST FUNCTIONAL SERVICING REPORT

**EDENSHAW ANN DEVELOPMENTS LIMITED** 

**FUNCTIONAL SERVICING REPORT** 

PROJECT NO.: 19M-00253 DATE: MAY 10, 2019

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### SIGNATURES



**REVIEWED BY** 

Alex Williams, P.Eng. Project Manager

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### 1 INTRODUCTION

#### 1.1 INTRODUCTION

WSP Canada Group Limited (herein called WSP) has been retained to prepare a Functional Servicing Report to assess the servicing requirements relating to the proposed development at 22-28 Ann Street and 78 Park Street East in the City of Mississauga. This report provides the conceptual framework for water distribution, sanitary sewage, and storm drainage for the development of this site. A Stormwater Management Report outlining the proposed stormwater quality and quantity controls on this site has been prepared under a separate cover, also by WSP Canada Group Limited.

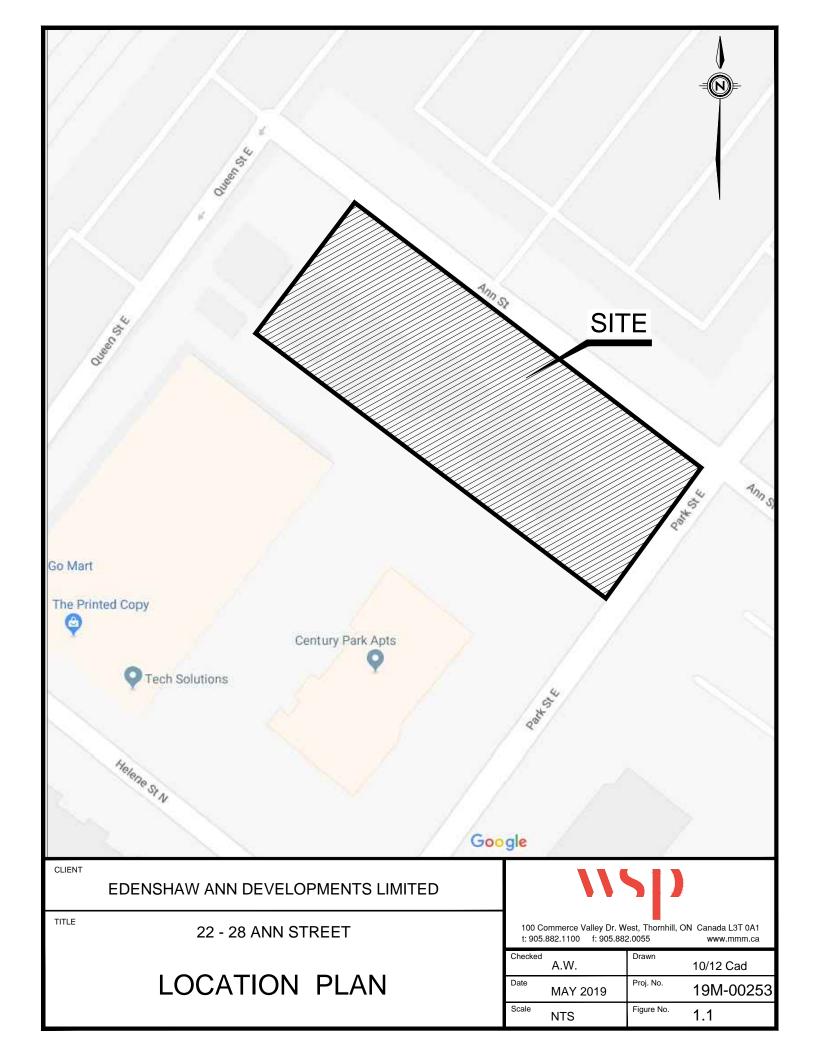
In preparing this report, WSP staff reviewed and secured available City of Mississauga and Region of Peel Plan and Profile Drawings, as well as the architectural site plans prepared by IBI Group Architects, a survey prepared by Tarasick McMillan Kubicki Limited, and SUE investigation by Multiview Locates Inc.

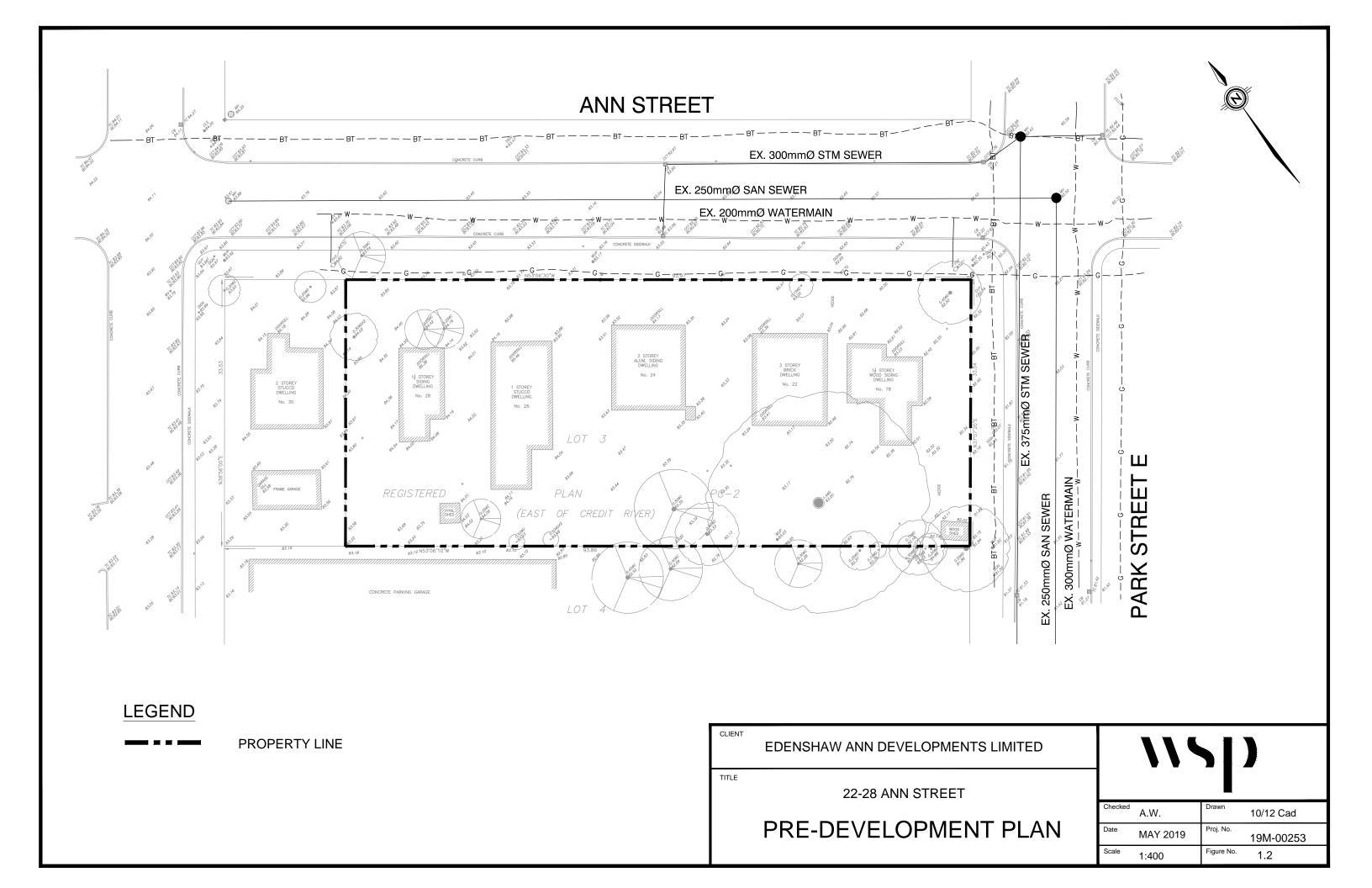
#### 1.2 SITE DESCRIPTION

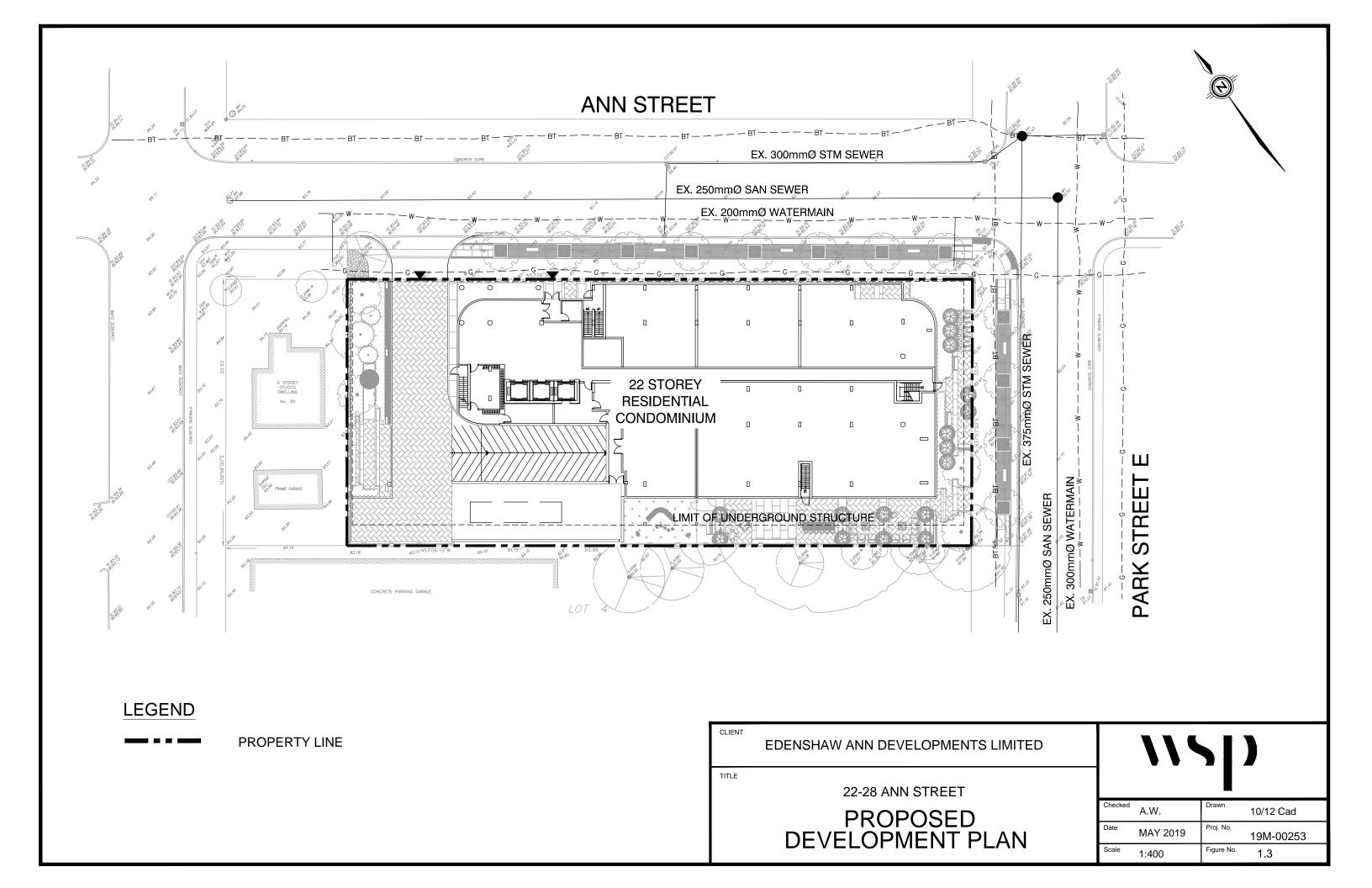
The site is a 0.26 ha parcel of land located at the west corner of Ann Street and Park Street East intersection, consisting of municipal addresses 22-28 Ann Street and 78 Park Street East. In the predevelopment condition the site is contains four detached single family residential homes as well as a 3 storey multi-unit apartment building.

The proposed site development includes a 22-storey residential condominium building with an estimated 313 residential units, 3 live/work units and 4 floors of below grade parking, covering the entire site.

The site will be serviced by existing local municipal sewers and watermains within the adjoining municipal right-of-ways. All existing service connections within the site will be decommissioned per Region of Peel and City of Mississauga Standards at the owner's cost. The proposed service connections will be extended to the underground parking foundation wall and coordinated with the building design team during detailed design. Refer to Figure 1.1 for the Location Map, Figure 1.2 for the Pre-development Site Condition and Figure 1.3 for an illustration of the Proposed Development Plan.







# 2 WATER SUPPLY AND APPURTENANCES

#### 2.1 EXISTING CONDITIONS

Locally, there is a 200 mm diameter watermain on Ann Street, and a 300 mm diameter watermain on Park Street East.

#### 2.2 WATER SUPPLY

In accordance with Region of Peel Standards, a 300 mm diameter watermain is required to service high density residential. Therefore, the proposed development will be serviced from the 300 mm diameter watermain on Park Street East. It is proposed to provide a 150 mm diameter domestic connection branching off a proposed 200 mm diameter fire service connection. The proposed connections will include valve and boxes at the property line. In addition, a water meter and a double detector check valve will be installed in the mechanical room within the building in accordance with the Region of Peel standards. The mechanical room will need to be accessible by the Region and provide remote read-out locations for the Region's use in reading the meters. Refer Figure 2.1 for proposed water servicing layout.

The estimated domestic water demand has been calculated using the Region of Peel Watermain Design Criteria and the site statistics provided by the architect. The Region of Peel Watermain Design Criteria also note that some new development can generate higher water demands during the first years of occupancy. Therefore, domestic water demands have been calculated for both the long term and the short term. For detailed calculations, see Appendix B;

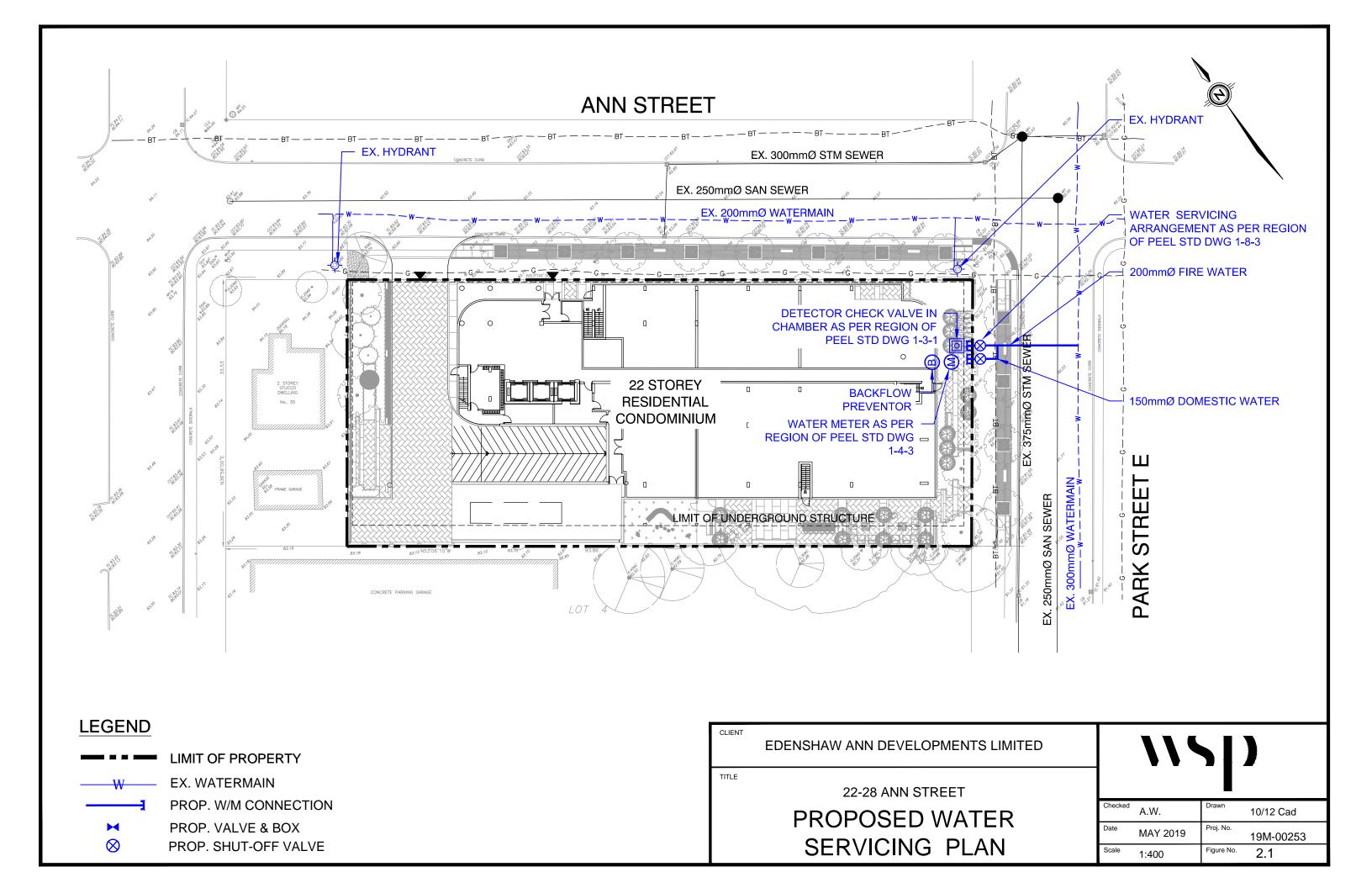
	Long Term	Short Term
Average Water Consumption Rate (Long Term)	280 litres/person/day	409 litres/person/day
Residential Apartment Units & Population Density	316 units / 2.7 people per unit	316 units / 2.7 people per unit
Total Residential Equivalent Population	854 people	854 people
Max Day Peaking Factor	2.0	2.0
Peak Hour Peaking Factor	3.0	3.0
Average Water Demand	2.77 L/s	4.04 L/s
Max Day Water Demand	5.54 L/s	8.09 L/s
Peak Hour Water Demand	8.30 L/s	12.13 L/s

The estimated fire flow has been calculated using the recommendations of the Fire Underwriters Survey. The fire flow calculation indicates that the recommended fire flow for this proposed development is  $\sim$ 6,841 L/min ( $\sim$ 1,805 US GPM). The results of these calculations are included in Appendix A.

Currently, there are two (2) existing hydrants in the vicinity of the proposed development. One is located near the south corner of Ann Street and Queen Street East intersection and the other is located near the west corner of Ann Street and Park Street East intersection. The proposed water servicing and existing hydrant locations are shown on Figure 2.1.

#### 2.3 HYDRANT FLOW TEST

At the time of preparing this report, a hydrant flow test has not been completed. The test will be scheduled and conducted in the near future and the results will be analyzed against the required flow demand of the proposed development described above and included in the Functional Servicing Report at such time.



## **3 SANITARY SEWAGE SYSTEM**

#### 3.1 EXISTING CONDITIONS

Locally, there is a 250 mm diameter sanitary sewer on Ann Street and a 250 mm dimeter sanitary sewer on Park Street East. The Ann Street sewer flows southeast to the Park Street East sewer, the Park Street East sewer flows southwest to the Helene Street North sewer, and southeast along Helene Street to the trunk sewer on Lakeshore Road East sewer.

#### 3.2 DESIGN PARAMETERS

The theoretical peak sanitary flows have been calculated using the following factors taken from the Region of Peel Sanitary Sewer Design Criteria, July 2009

- ► 50 ppl/ha (Single Family > 10m frontage)
- ► 70 ppl/ha (Single Family < 10m frontage)
- ► 70 ppl/ha (Semi-Detached)
- ► 175 ppl/ha (Row Dwellings)
- ► 475 ppl/ha (Apartments)
- ▶ 2.7 people per unit (For apartments with density greater than 475 ppl/ha)
- ▶ 302.8 L/cap/day average day flow generation rate
- ► Peaking Factor Harmon Peaking Factor
- ► Infiltration = 0.0002m³/s/ha

#### 3.3 EXISTING FLOW TO SANITARY SEWER

Based on the design criteria noted above, it is estimated that in the pre-development condition the site discharged an average of 0.10 L/s to the sanitary sewer system and a peak of 0.25 L/s to the sanitary sewer system, including infiltration. Refer to Appendix B for detailed pre-development sanitary flow rate calculations.

#### 3.4 POST DEVELOPMENT SANITARY SEWER FLOW

An estimate of the post-development sanitary sewage flows to the downstream sanitary sewer system has been calculated based on the Region of Peel Sanitary Sewer Design Criteria and the preliminary site statistics provided by the architect. A summary of the calculations can be found below;

Sanitary Demand Rate	302.8 litres/person/day
Residential Population	854 people
Avg. Residential Flow	2.99 L/s
Infiltration	No infiltration (Entire site UG Parking)
Average Sanitary Flow from Site	2.99L/s
Peaking Factor	Residential: Harmon Peaking Factor (3.84)
Peak Sanitary Flow from Site	11.50 L/s
Net Sanitary Flow Increase in Peak Sanitary Flow from Site to Sanitary Sewer System	11.25 L/s (11.50 L/s – 0.25 L/s)

Refer Appendix B for site statistics and detailed pre- and post-development flow calculations.

#### 3.5 DOWNSTREAM SANITARY SEWER CAPACITY ANALYSIS

WSP has prepared a pre- and post-development downstream sanitary sewer analysis. The analysis includes calculations for the wet weather flow condition, where an infiltration (0.20 L/s/ha) has been added to the calculated sanitary flow. The sanitary flow for the sewershed was calculated using the Region of Peel Sanitary Sewer Design Criteria as outlined in Section 3.2. The sanitary generation from the site outlined in Section 3.4 was applied to the pre-development analysis to form the analysis of the post-development conditions. See Appendix C for the Sanitary Sewer Design Sheets. To facilitate this analysis, a Sanitary Sewer Drainage Area Plan has been created and is located in Appendix C.

A development application for the 21-29 Park Street East site has been submitted, and it is expected that the site will be developed in the near future. Therefore, the post-development sanitary flow, calculated based on the Region of Peel design

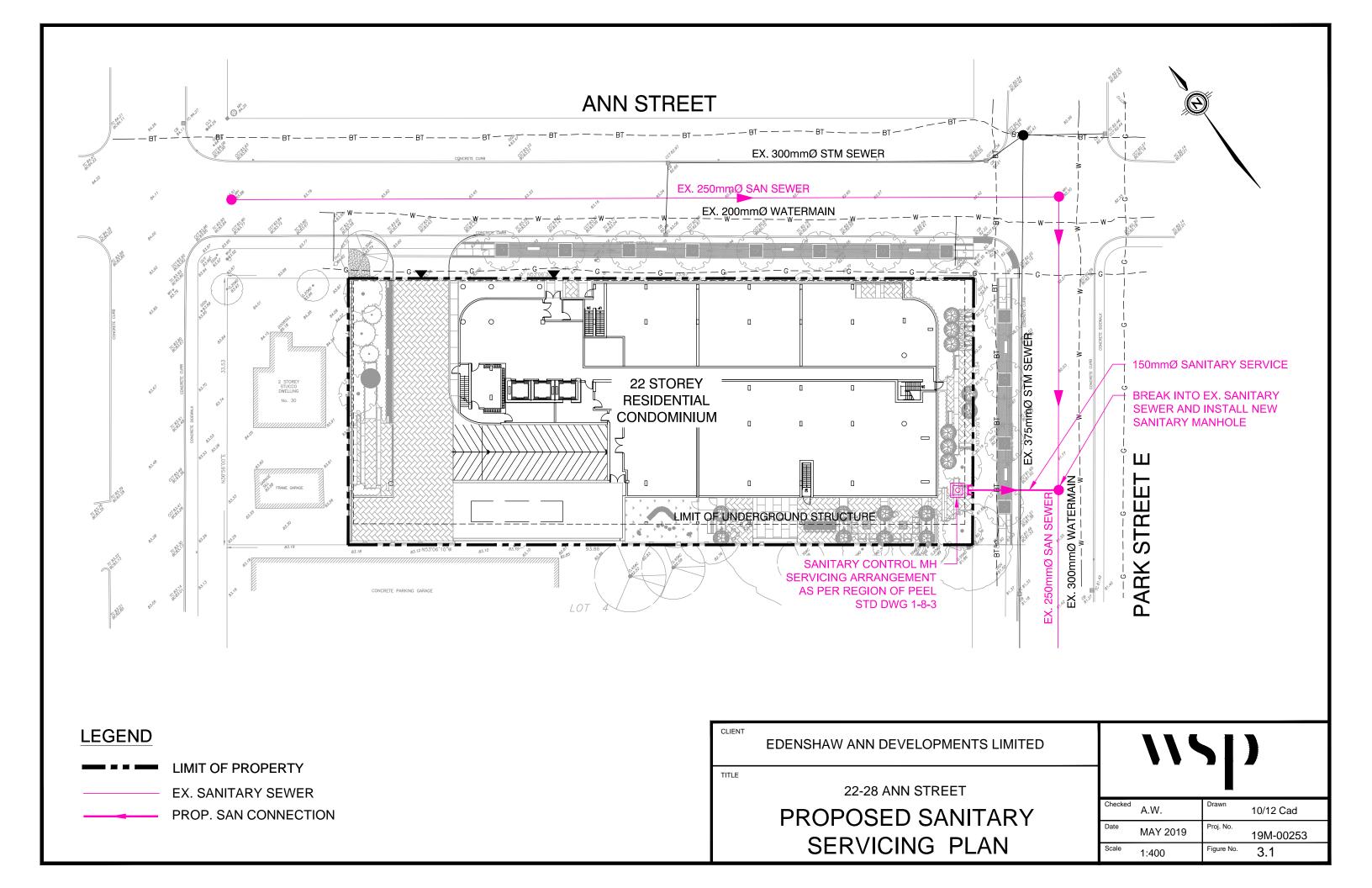
criteria and site statistics provided by the architect, has been included as an existing sanitary flow for the purpose of analyzing receiving sewer capacity.

In the post development condition, the analysis demonstrates that the existing municipal sewer system has adequate capacity to support the addition of 11.25 L/s of flow from the proposed development without surcharging in any leg. Consequently, WSP Group concludes that the existing municipal sewer can accept the flow from the proposed site and no external sewer improvements are required.

#### 3.6 SANITARY SERVICE

It is proposed to service the site with a 150 mm diameter PVC sanitary service connected to the existing 250 mm sanitary sewer on Park Street East. A control manhole will be placed immediately inside the underground parking structure.

The internal sanitary sewer system within the parking structure will be designed by the mechanical engineer. Proposed sanitary sewers within the private site will be designed to meet Ontario Plumbing Code Standards. The sanitary service connection to the site within the existing municipal road allowance will be designed to the Region of Peel Standards. Refer to Figure 3.1 for proposed sanitary servicing layout.



### 4 STORM DRAINAGE

#### 4.1 STORMWATER MANAGEMENT REPORT

A Stormwater Management Report for this development has been prepared under a separate cover. It identifies the stormwater quantity and quality controls under which this site will operate.

#### 4.2 EXISTING CONDITIONS

The existing storm sewer in the vicinity of the site is a 375mm diameter storm sewer on Park Street East.

#### 4.3 PROPOSED DEVELOPMENT

The proposed development covers the majority of the site and as noted, includes a 22-storey residential building and below grade parking. All storm flows from the site will be captured and directed to a stormwater storage tank. The tank will be sized to reduce the 100-year post-development flows to the 2-year pre-development levels. The tank will have an access hatch which is accessible from the surface which will also double as an emergency overflow. For detailed storage and storm flow calculations, refer to separate Stormwater Management Report prepared by WSP.

#### 4.4 GRADING

#### 4.4.1 EXISTING CONDITIONS

WSP reviewed the topographical survey prepared Tarasick McMillan Kubicki Limited to determine the existing drainage patterns. Our review indicated that the site primarily drains south to Park Street East. Specifically, the existing buildings have a split drainage pattern, with the fronts of the buildings draining to Ann St and the rears of the buildings draining to Park Street East.

#### 4.4.2 PROPOSED CONDITIONS

The Ann Street and Park Street East boulevards, adjacent to the proposed development, will be regraded to a 2.0% cross fall towards the roads, while maintaining the existing bottom of curb elevations. The existing elevations along the north and west property lines promote the overland drainage away from the proposed development and, therefore, will not require any changes to the grading design.

Refer to Figure 4.2 for the preliminary proposed grading.

#### 4.5 MINOR STORM DRAINAGE SYSTEM

The storm flows will be directed to the stormwater cistern and controlled to an allowable release rate, which has been set to be equal to a 2-year storm in the pre-development condition.

It is proposed to provide a new 200 mm diameter storm connection that will connect to the existing 375 mm diameter storm sewer on Park Street East. A control manhole is proposed to be placed immediately inside the property line. The control manhole and cistern will be accessible at grade outside the building.

The new storm connection within the Park Street East right-of-way will be designed to the standards and specifications of the City of Mississauga. The new on-site storm sewers, which will be located within the parking garage, will be designed by a mechanical engineer to meet the standards of the Ontario Building Code. Refer Figure 4.1 for the proposed storm sewer layout.

#### 4.6 MAJOR STORM DRAINAGE SYSTEM

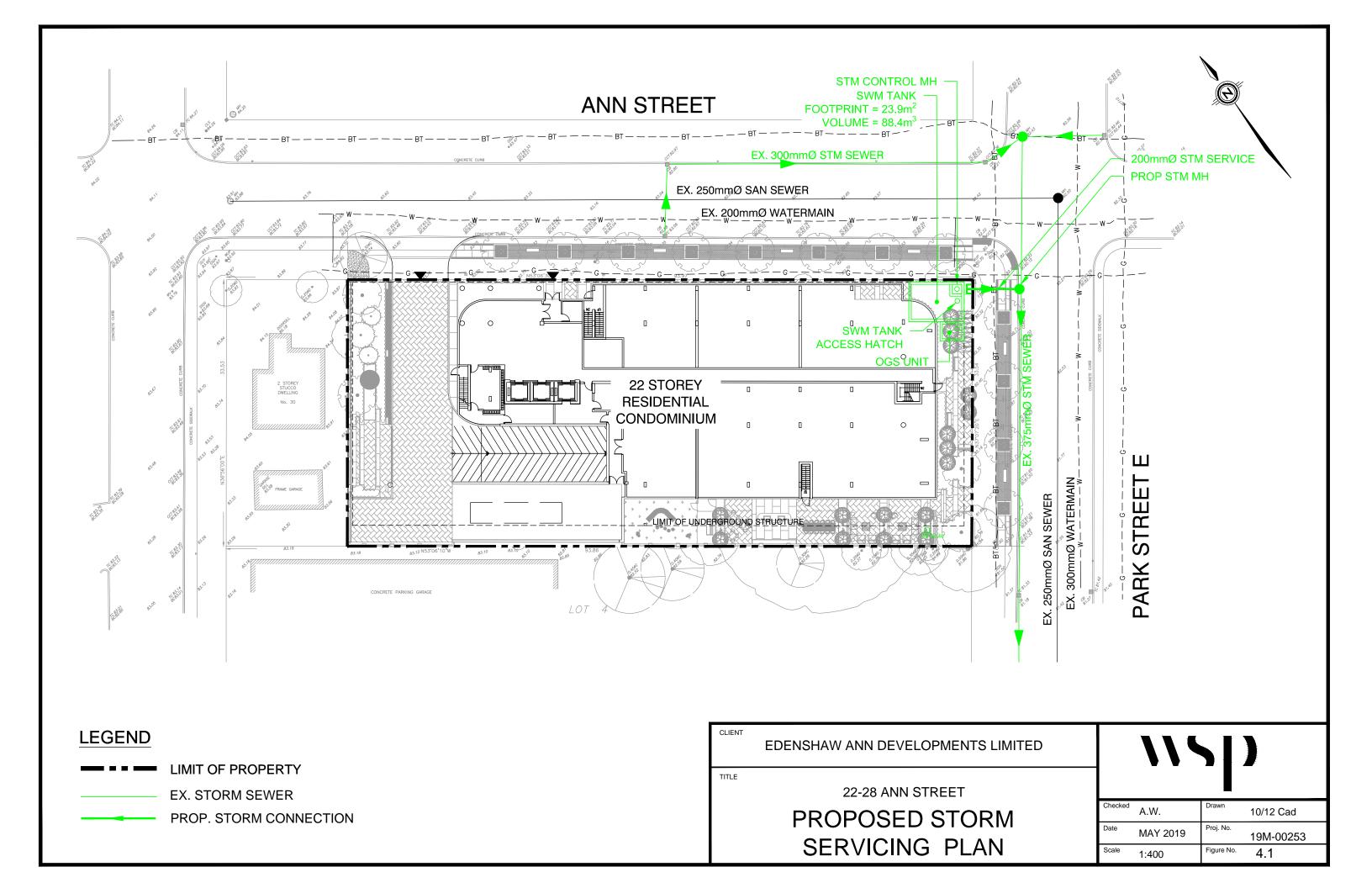
The storm flows will be collected by on site area drains and catchbasins connected to an internal storm drainage system and directed into the stormwater storage tank. The flow will be controlled by a flow control device and released to the City's storm sewer at the controlled release rate. In case of system failure, the system has been designed to have an emergency overflow access to the surface. Since all storm flows, up to 100-year storm events, will be reduced to the 2-year pre-development levels, the existing storm sewer system will not be adversely affected by the post-development condition.

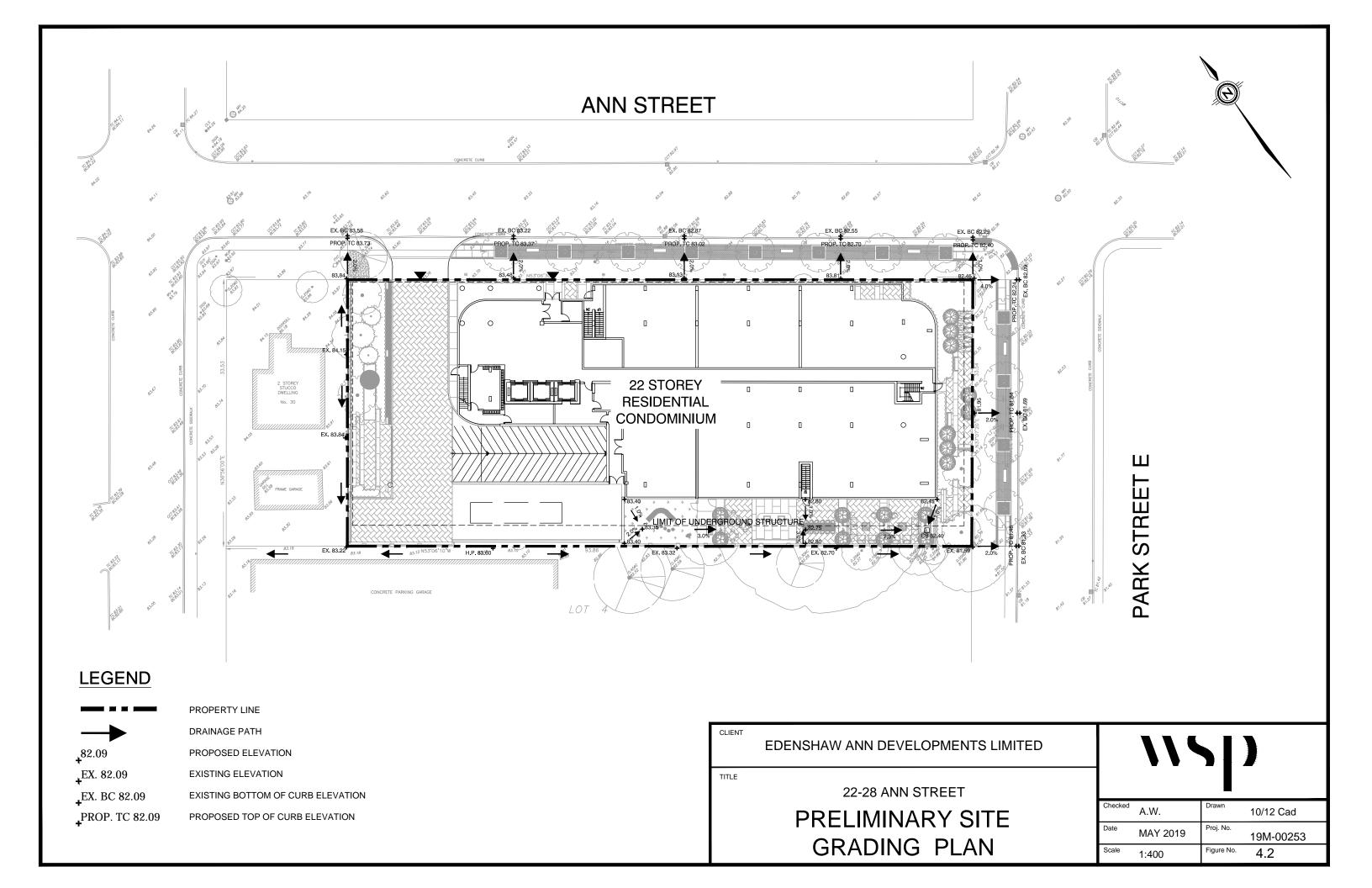
#### 4.7 DOWNSTREAM STORM SEWER CAPACITY ANALYSIS

WSP has prepared a pre- and post-development downstream storm sewer analysis. The analysis includes calculations for a 10-year design storm. The storm flow for the sewershed was calculated using the City of Mississauga Storm Sewer Design Criteria. The controlled storm release rate from the site was applied to the pre-development analysis to form the analysis of the post-development conditions. See Appendix C for the Storm Sewer Design Sheets. To facilitate this analysis, a Storm Sewer Drainage Area Plan has been created and is located in Appendix D.

In the pre-development conditions the design sheet shows that all downstream sewer legs in the sewershed are surcharged. Acknowledging this, the proposed development has proposed to control the storm flow from the site to the 2-year pre-development level for all storm events up to the 100-year storm. This means that during all storm events greater than a 2-year storm, including the 10-year event for which the sewers are to be designed there will be less flow in the downstream sewers as a result of this development and the surcharge in the sewers will be reduced as a result. To demonstrate this, a pre-development and post-development HGL analysis has been conducted and is included in Appendix D. The results of the HGL analysis show that the HGL is lowered in all downstream sewer legs. Therefore, since the development is improving

ne surcharge condition in the existing sewers WSP has concluded that no external sewer improvements are required a esult of this development.	s a





### 5 CONCLUSIONS

#### 5.1 WATER

The proposed water servicing for the site will include a 150 mm diameter domestic water connection branching off a 200 mm diameter fire water connection. The water service connections will be made to the existing 300 mm watermain on Park Street East. A hydrant flow test will be conducted to verify that the existing watermain has adequate capacity to support the proposed development.

#### 5.2 SANITARY

The proposed sanitary servicing for the site will include a 150 mm diameter sanitary service connecting to the existing 250 mm diameter sanitary sewer on Park Street East. The downstream sanitary sewer capacity analysis demonstrates that the existing sanitary sewer system has adequate capacity to accept the estimated post-development flows from the development without surcharging in any leg.

#### 5.3 STORM

The proposed storm servicing for the site will include a 200 mm diameter storm service connecting to the existing 375 mm diameter storm sewer on Park Street East. A downstream storm sewer capacity analysis and HGL analysis has been conducted that demonstrates that the existing storm sewer system is surcharged, however the stormwater management control proposed as part of this development will reduce the storm flows from the site and reduce the surcharge in all of the downstream storm sewer legs.

## **APPENDIX**

# FUS CALCULATIONS

#### **APPENDIX A**

#### FIRE FLOW CALCULATIONS

Project: 22-28 Ann Street Job No.: 19M-00253

Fire flow required for a given area based on Fire Underwriters Survey (FUS) Water Supply for Public Fire Protection (1999)

$$F = 220 \ C \sqrt{A}$$

where

F = Fire flow in Litres per minute (Lpm)

C = coefficient related to the type of construction

A = total floor area in square metres

#### Calculations per FUS

1. Estimate of Fire Flow

C = 0.6 for fire resistive construction

A = 2810.8 m2 (largest GFA plus 25% of GFA for two immediately adjoining floors)

6,998 Lpm F=

2. Occupancy Reduction

15% reduction for "Non-Combustible" Occupancy

3. Sprinkler Reduction

30% reduction for NFPA Sprinkler System

Separation Charge 4.

Face	Distance (m)	Charge	
West Side	2	25%	
East Side	46	0%	
North Side	8	20%	
South Side	46	0%	
	Total	45% o	f

F = 4164 + 2677 6,841 Lpm (2,000 Lpm < F < 45,000 Lpm; OK)

F = 1,805 US GPM 114 L/s

Notes

Date Printed: 01/05/2019

5,948 = 2,677 Lpm

## **APPENDIX**

# B DOMESTIC WATER DEMAND AND SANITARY FLOW CALCULATIONS

# APPENDIX B 22-28 ANN STREET Pre-Development Site Statistics

#### **Residential Units**

Unit Type	Area (ha)	Pop Density (ppl/ha)		Population	
SF Homes	0.26		50		13

**Note:** Population calculated per Region of Peel Sanitary Sewer Design Criteria Section 2.1. The predevelopment site consists of 3 single family homes on a combined 0.26ha of land. The population was based on a population density of 50 ppl/ha for SF homes.

#### **Pre-Development Sanitary Flow**

Res Population = 13

Avg Res Flow = 0.05 L/s (assumes 302.8L/cap/d)

Res Peak Factor = 4.40 (Harmon Formula)

Peak Res Flow = 0.20 L/s

Infiltration = 0.05 L/s

Total Avg San Flow = 0.10 L/s
Total Peak San Flow = 0.25 L/s

#### **Pre-Development Water Demand**

Res Population = 13

Avg Res Demand = 0.04 L/s (assumes 280L/cap/d)

 Max Day Factor =
 2.00

 Max Day Flow =
 0.09 L/s

 Peak Hour Factor =
 3.00

 Peak Hour Flow =
 0.13 L/s

# APPENDIX B 22-28 ANN STREET Post-Development Site Statistics

#### **Residential Units**

Unit Type	Quantity	Pop Density	Population
Res. Units	316	2.7	854

**Note:** Population calculated per Region of Peel Sanitary Sewer Design Criteria Section 2.1. As the population density of the site is expected to be greater than 475ppl/haa factor of 2.7ppl/unit was used.

#### **Post-Development Sanitary Flow**

Res Population = 854

Avg Res Flow = 2.99 L/s (assumes 302.8L/cap/d)

Res Peak Factor = 3.84 (Harmon Formula)

Peak Res Flow = 11.50 L/s

Total Avg San Flow = 2.99 L/s
Total Peak San Flow = 11.50 L/s

#### Post-Development Water Demand - Short Term

Res Population = 854

Avg Res Demand = 4.04 L/s (assumes 409L/cap/d)

 Max Day Factor =
 2.00

 Max Day Flow =
 8.09 L/s

 Peak Hour Factor =
 3.00

 Peak Hour Flow =
 12.13 L/s

 Fire Flow =
 114 L/s

Fire Flow = 114 L/s
Maximum Day + Fire Flow = 122.09 L/s

#### Post-Development Water Demand - Long Term

Res Population = 854

Avg Res Demand = 2.77 L/s (assumes 280L/cap/d)

 Max Day Factor =
 2.00

 Max Day Flow =
 5.54 L/s

 Peak Hour Factor =
 3.00

 Peak Hour Flow =
 8.30 L/s

 Fire Flow =
 114 L/s

Maximum Day + Fire Flow = 119.54 L/s

## **APPENDIX**

# SANITARY SEWER DRAINAGE PLANS AND DESIGN SHEETS

#### THE REGIONAL MUNICIPALITY OF PEEL SANITARY DESIGN CHART 22-28 ANN STREET - CITY OF MISSISSAUGA PRE-DEVELOPMENT CONDITION

WSP CANADA GROUP LIMITED

DRAINAGE AREA PLAN NO.:

\* DESIGN FLOWS AS PER REGION OF

PEEL SANITARY SEWER DESIGN FLOW

DATE: MAY 2019
DESIGNED BY:

Manning's n= 0.013 CHECKED BY:

					1		1	DESIGN	Docking	DEAK	INFILTRATION	TOTAL			1	1	1		1
LOCATION	FROM	то	AREA	AREA	POP.	симм.	симм.	DESIGN SEWAGE	Peaking Factor	PEAK SEWAGE	FLOW *	TOTAL FLOW	LENGTH	GRADIENT	PIPE SIZE	CAPACITY		VELOCITY	VELOCITY
2007.11.014	MH	мн	744274	DENSITY		AREA	POP.	FLOW	1 40101	FLOW	0.200	. 2011	22.10.11	Old (Diz.)	1 2 0.22	677.6	% FULL	FULL	ACTUAL
			(ha)	(ppha)		(ha)		(L/sec)		(L/sec)	(L/sec/ha)	(L/sec)	(m)	(%)	(mm)	(L/sec)		(m/sec)	(m/sec)
21-29 Park St Development					559 10														
			0.19 1.43	50 475	679														
Park St E	149	150	1.62		1248	1.62	1248	4.37	3.74	16.3	0.3	16.6							
Elizabeth St	North	150	1.06	475	504	1.06	504	1.8	3.97	7.0	0.2	7.2			-				
			0.36	50	18														
			0.56	475	266														
Park St E	East	150	0.92		284	0.92	284	1.0	4.09	4.1	0.2	4.3							
Elizabeth St	150	147	0.63	475	299	4.23	2335	8.2	3.53	28.9	0.8	29.7							
	-																		
Elizabeth St North	South	147	0.10	475	48	0.10	48	0.2	4.32	0.7	0.0	0.7							
High Street E	West	147	0.82	475	390	0.82	390	1.4	4.03	5.5	0.2	5.7							
High St E	147	157	0.18	475	86	5.33	2857	10.0	3.46	34.6	1.1	35.7							
High St E	157	155A	0.72	475	342	6.05	3199	11.2	3.42	38.3	1.2	39.5							
High St E	155A	155	0.00	0	0	6.05	3199	11.2	3.42	38.3	1.2	39.5							
			0.44	475	77														-
Death Of E	East	170	0.44	175 50	29	1.01	106	0.4	4.24	1.6	0.2	1.8							
Park St E	Last	170	0.57	30	2.5	1.01	100	0.4	7.27	1.0	0.2	1.0		<del></del>					
			0.21	50	11														
EXISTING SITE	171	170	0.26	50	13	0.47	24	0.1	4.37	0.4	0.1	0.5	104.0	1.14	250	63.4	0.72%	1.29	0.39
Park St E	170	153	1.26	475	599	2.74	728	2.5	3.88	9.9	0.5	10.4	119.6	0.68	250	49.0	21.21%	1.00	0.78
Helene St N	North	153	0.94	475	447	0.94	447	1.6	4.00	6.3	0.2	6.5							
Helene St N	153	153A	0.00	0	0	3.68	1174	4.1	3.75	15.4	0.7	16.1	23.9	4.67	250	128.5	12.53%	2.62	1.73
Helene St N	153A	155A 154	0.00	0	0	3.68	1174	4.1	3.75	15.4	0.7	16.1	42.0	4.67	250	128.5	12.53%	2.62	1.73
Helene St N	154	155	0.00	0	0	3.68	1174	4.1	3.75	15.4	0.7	16.1	55.0	0.50	250	42.0	38.29%	0.86	0.81
					1			1				1							
			1.35	475	641														
			0.80	50	40														
High St E	East	155	0.96	475	456	3.11	1137	4.0	3.76	15.0	0.6	15.6							
Helene St N	455	Labasha	0.00	475	440	40.77	5050	00.0	0.47	00.0	0.0	20.0	405.0	0.00	450	450.0	44.400/	0.00	0.04
Helene St N	155	Lakeshore	0.93	475	442	13.77	5952	20.9	3.17	66.2	2.8	69.0	125.8	0.30	450	156.2	44.19%	0.98	0.94
			l .				l		l	l			l		l	L			

NOTE: (1) - Grey rows are not receiving sewers and flows are unchanged by the proposed development.

## THE REGIONAL MUNICIPALITY OF PEEL SANITARY DESIGN CHART 22-28 ANN STREET - CITY OF MISSISSAUGA POST-DEVELOPMENT CONDITION

WSP CANADA GROUP LIMITED

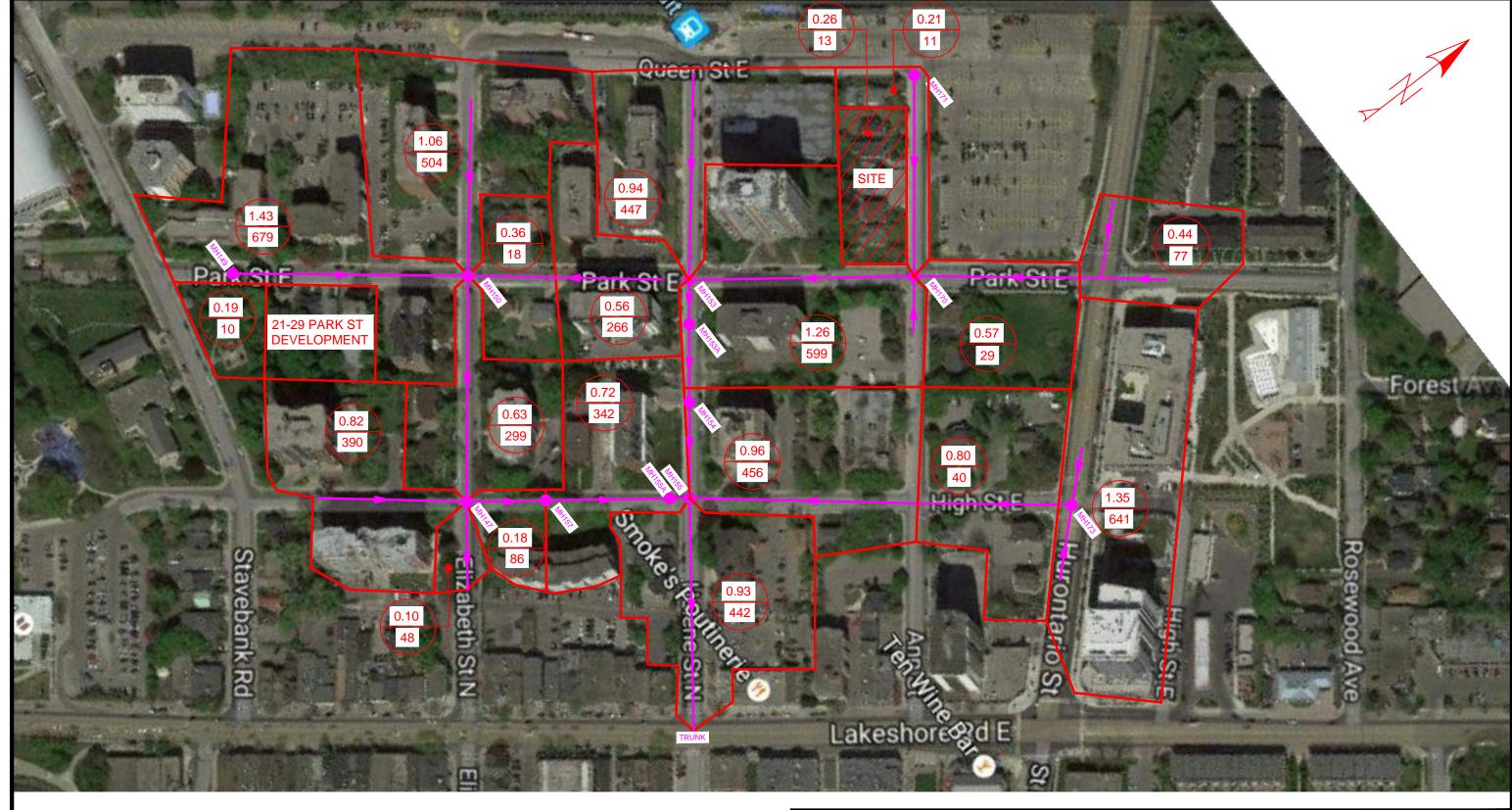
\* DESIGN FLOWS AS PER REGION OF PEEL SANITARY SEWER DESIGN FLOW

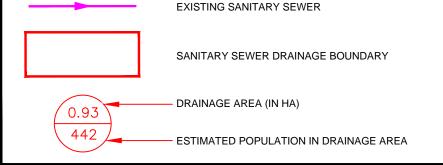
DATE: MAY 2019 DESIGNED BY:

DRAINAGE AREA PLAN NO.: CHECKED BY: Manning's n= 0.013

LOCATION	FROM MH	то мн	AREA (ha)	AREA DENSITY (ppha)	POP.	CUMM. AREA (ha)	CUMM. POP.	DESIGN SEWAGE FLOW (L/sec)	Peaking Factor	PEAK SEWAGE FLOW (L/sec)	INFILTRATION FLOW * 0.200 (L/sec/ha)	TOTAL FLOW (L/sec)	LENGTH (m)	GRADIENT (%)	PIPE SIZE	CAPACITY (L/sec)	% FULL	VELOCITY FULL (m/sec)	VELOCITY ACTUAL (m/sec)
21-29 Park St Development					559														
·			0.19	50	10														
			1.43	475	679														
Park St E	149	150	1.62		1248	1.62	1248	4.37	3.74	16.3	0.3	16.6	113.5	0.38	250	36.7	45.28%	0.75	0.72
Elizabeth St	North	150	1.06	475	504	1.06	504	1.8	3.97	7.0	0.2	7.2							
			0.36	50	18														
			0.56	475	266														4
Park St E	East	150	0.92		284	0.92	284	1.0	4.09	4.1	0.2	4.3							
Elizabeth St	150	147	0.63	475	299	4.23	2335	8.2	3.53	28.9	0.8	29.7	123.0	0.50	250	42.0	70.75%	0.86	0.93
Elizabeth St North	South	147	0.10	475	48	0.10	48	0.2	4.32	0.7	0.0	0.7							
High Street E	West	147	0.82	475	390	0.82	390	1.4	4.03	5.5	0.2	5.7							
High St E	147	157	0.18	475	86	5.33	2857	10.0	3.46	34.6	1.1	35.7	40.0	0.30	375	96.0	37.19%	0.87	0.81
High St E	157	155A	0.72	475	342	6.05	3199	11.2	3.42	38.3	1.2	39.5	70.0	0.47	375	120.2	32.89%	1.09	0.96
High St E	155A	155	0.00	0	0	6.05	3199	11.2	3.42	38.3	1.2	39.5	13.0	0.47	375	120.2	32.89%	1.09	0.96
	East	170	0.44	175 50	77 29	1.01	106	0.4	4.24	1.6	0.2	1.8							
Park St E	East	170	0.57	50	29	1.01	100	0.4	4.24	1.0	0.2	1.0						===	
Ann St	171	170	0.21	50	11	0.21	11	0.0	4.41	0.2	0.0	0.2	104.0	1.14	250	63.4	0.32%	1.29	0.39
PROPOSED DEVELOPMENT					854 <sup>(1)</sup>														+
Park St E	170	153	1.26	475	599	2.48	1569	5.5	3.67	20.1	0.5	20.6	119.6	0.68	250	49.0	42.01%	1.00	0.95
Helene St N	North	153	0.94	475	447	0.94	447	1.6	4.00	6.3	0.2	6.5							
Helefie St N	Notui	100	0.94	475	447	0.94	447	1.0	4.00	0.3	0.2	0.5						===	
Helene St N	153	153A	0.00	0	0	3.42	2015	7.1	3.58	25.3	0.7	26.0	23.9	4.67	250	128.5	20.23%	2.62	1.99
Helene St N	153A	154	0.00	0	0	3.42	2015	7.1	3.58	25.3	0.7	26.0	42.0	4.67	250	128.5	20.23%	2.62	1.99
Helene St N	154	155	0.00	0	0	3.42	2015	7.1	3.58	25.3	0.7	26.0	55.0	0.50	250	42.0	61.83%	0.86	0.91
			1.35	475	641														
			0.80	50	40														
High St E	East	155	0.96	475	456	3.11	1137	4.0	3.76	15.0	0.6	15.6					-		
Helene St N	155	Lakeshore	0.93	475	442	13.51	6793	23.8	3.12	74.3	2.7	77.0	125.8	0.30	450	156.2	49.31%	0.98	0.97

NOTE: (1) - For population of proposed development see Appendix B Post-Development Site Statistics (2) - Grey rows are not receiving sewers and flows are unchanged by the proposed development.





CLIENT **EDENSHAW DEVELOPMENTS LIMITED** 

22-28 ANN STREET

SANITARY SEWER DRAINAGE PLAN

1150	
100 Commerce Valley Dr. West, Thornhill, ON Canada L3T 0A1	
t: 905.882.1100 f: 905.882.0055 www.mmm.ca	

Checked	A.K.	Drawn	10/12 Cad
Date	MAR 2019	Proj. No.	19M-00253
Scale	NTS	Figure No.	SAN-1

## **APPENDIX**

# STORM SEWER DRAINAGE PLANS AND DESIGN SHEETS

DEVELOPMENT	22-28 ANN STREET
CONSULTANT	WSP Canada Group Limited

MAJOR DRAINAGE AREA

MISSISSAUGA
Transportation and Works
STORM DRAINAGE DESIGN CHART
FOR CIRCULAR DRAINS FLOWING FULL

SHEET	1	of	1
DESIGNED BY		IB	
OUEOKED DV		A 1/	

#### 10 YEAR PRE-DEVELOPMENT STORM DESIGN SHEET

							11	JILANT	INC-DEVE	LOFIVILIV	11 3101	IN DESIGN	SIILLI											
LOCATION OF SITE	⊠ From Upstream #	M To Downstream	(a) Adjacent Contributary Area	(b) ✓ Total Contributary Area	O Runoff Coefficient	> Area Times Runoff C Coefficient	Accumulated Area  A Times Runoff  C Coefficient for Section	Time of Concentration at Upstream End of Section	By P Flow Time within Section	Time of Doncentration at Concentration at Downstream End of Section	BB Intensity of Rainfall (10 Year Event)	B C Quantity of Flow to be composed in (s Section Section C)	TOTAL Quantity of  TOTAL Quantity of  Flow to be  Accomodated in  Section	Manning's ⊃ Roughness Coefficient	s Slope	(sequoni) O Nominal Diameter	(B) O Nominal Diameter	(#) T Length of Section	∃ ⊢ Length of Section	S Velocity of Flow with S Pipe Flowing Full	(s) Capacity of Pipe	SURCHARGED?	(3) % FREE	t Time of Flow in (ui, //, Section
			(na)	(Hu)				(11111)	(11111)	(11111)	(111117 111)	(111 7 8)	(111 7 5)		(70)	(ITIOTICS)	()	(11)	(111)	(1117-0)	(111 7 8)		(,	(11111)
High Rise			1.35		0.90	1.22																		
SF Homes			0.33		0.55	0.18																		
Park Street E (Total)			1.68	1.68		1.40	1.40																	
Park Street E (1/3)	23	25	0.56	0.56		0.47	0.47	15.00	0.39	15.39	99.17	0.129	0.129	0.013	1.54	12.00	300	130	39.6	1.698	0.120	SURCHARGED	-7.71%	0.39
Park Street E (1/3)	25	26	0.56	1.12		0.47	0.93	15.39	0.25	15.64	97.66	0.255	0.255	0.013	0.81	12.00	300	60	18.3	1.231	0.087	SURCHARGED	-192.51%	0.25
Park Street E (1/3)	26	27	0.56	1.68		0.47	1.40	15.64	0.30	15.94	96.72	0.378	0.378	0.013	0.81	18.00	450	95	29.0	1.613	0.257	SURCHARGED	-47.40%	0.30
Park Street E	27	35	0.00	1.68		0.00	1.40	15.94	0.05	15.99	95.62	0.374	0.374	0.013	1.25	18.00	450	20	6.1	2.004	0.319	SURCHARGED	-17.30%	0.05
High Rise			1.14		0.90	1.03																		
SF Homes			0.58		0.55	0.32																		
Upstream of MH35	Upstream	35	1.72	1.72		1.35	1.35																	
-																								
High Rise			0.44		0.90	0.40																		
Dense Housing			0.22		0.65	0.14																		
Elizabeth Street (Total)			0.66	0.66		0.54	0.54																	
Elizabeth Street (1/3)	35	37	0.22	3.62		0.18	2.92	15.99	0.78	16.77	95.44	0.781	0.781	0.013	0.47	24.00	600	230	70.1	1.489	0.421	SURCHARGED	-85.45%	0.78
Elizabeth Street (1/3)	37	40	0.22	3.84		0.18	3.10	16.77	0.20	16.98	92.69	0.805	0.805	0.013	0.47	24.00	600	60	18.3	1.489	0.421	SURCHARGED	-91.19%	0.20
Elizabeth Street (1/3) Elizabeth Street	40 42	42 21	0.22	4.06 4.06		0.18	3.28 3.28	16.98 17.35	0.38	17.35 17.44	92.01 90.78	0.845 0.834	0.845 0.834	0.013	0.47	24.00	600 600	110 25	33.5 7.6	1.489	0.421 0.407	SURCHARGED SURCHARGED	-100.77% -104.73%	0.38
Elizabeth Street	44	21	0.00	4.00		0.00	3.20	17.55	0.09	17.44	90.76	0.034	0.034	0.013	0.44	24.00	000	2.5	7.0	1.440	0.407	SUNCHARGED	-104.7376	0.09
High Rise/Commercial			4.40		0.90	3.96																		
Park			0.20		0.30	0.06																		
Upstream of MH21	Upstream	21	4.60	4.60		4.02	4.02																	
High Street E (Total)			1.00	1.00	0.90	0.90	0.90																	
High Street E (1/2)	21	48	0.50	9.16	0.00	0.45	7.75	17.44	0.92	18.35	90.50	1.964	1.964	0.013	0.30	33.00	825	265	80.8	1.471	0.786	SURCHARGED	-149.79%	0.92
High Street E (1/2)	48	50	0.50	9.66		0.45	8.20	18.35	0.60	18.96	87.67	2.013	2.013	0.013	0.30	33.00	825	175	53.3	1.471	0.786	SURCHARGED	-156.03%	0.60
Single Family			0.06		0.55	0.03																	<u> </u>	
Parking Lot			0.91		0.90	0.82																	<u> </u>	
EXISTING SITE			0.26		0.55	0.14																		
Ann Street	68 70	70 72				0.99	0.99	15.00 15.39	0.39	15.39	99.17 97.65	0.275 0.271	0.275 0.271	0.013	1.54	12.00	300 300	131	39.9 6.1	1.698	0.120	SURCHARGED SURCHARGED		0.39
Ann Street	70	12	0.00			0.00	0.99	15.39	0.07	15.46	97.05	0.271	0.271	0.013	1.25	12.00	300	20	6.1	1.530	0.108	SURCHARGED	-150.36%	0.07
Park Street E (Total)			0.80		0.90	0.72																		
Park Street E (1/3)	72	74				0.24	1.23	15.46	0.53	15.99	97.39	0.335	0.335	0.013	1.32	15.00	375	190	57.9	1.824	0.201	SURCHARGED	-66.51%	0.53
Park Street E (1/3)	74	76				0.24	1.47	15.99	0.38	16.36	95.44	0.393	0.393	0.013	1.04	15.00	375	120	36.6	1.619	0.179	SURCHARGED	-119.69%	0.38
Park Street E (1/3)	76	66				0.24	1.71	16.36	0.31	16.67	94.10	0.451	0.451	0.013	0.95	18.00	450	105	32.0	1.747	0.278	SURCHARGED	-62.13%	0.31
Helene St N	North	66	1.76		0.90	1.58	1.58																	
Halana Ct M (T-4-1)			0.42		0.90	0.38																		
Helene St N (Total) Helene St N (1/4)	66	78	0.42		0.90	0.38	3.39	16.67	0.35	17.02	93.04	0.883	0.883	0.013	1 75	24.00	600	200	61.0	2.873	0.812	SURCHARGED	-8.68%	0.35
Helene St N (1/4)	78	80				0.09	3.48	17.02	0.33	17.02	91.85	0.896	0.896	0.013		24.00	600	175	53.3	2.848	0.805	SURCHARGED	-11.24%	0.33
Helene St N (1/4)	80	50				0.09	3.58	17.34	0.04	17.37	90.83	0.910	0.910	0.013	1.72		600	20	6.1	2.848	0.805	SURCHARGED	-12.99%	0.04
Helene St N (1/4)	50	97				0.09	11.87	18.96	0.13	19.09	85.91	2.856	2.856	0.013	0.25		1,200	45	13.7	1.724	1.949	SURCHARGED	-46.50%	0.13
			0.43		0.55	0.24																		
High Street E	East	97	2.17		0.90	1.95	2.19																	
Helene Street N	97	Trunk	0.81	0.81	0.90	0.73	14.79	19.09	1.16	20.25	85.53	3.542	3.542	0.013	0.25	48 00	1,200	230.0	120.0	1.724	1.949	SURCHARGED	-81.72%	1.16
THORNE GUIDEL IN	37	Truin	3.01	3.01	0.00	5.75	17.73	10.00	1.10	20.20	55.55	0.042	5.572	0.010	0.20	40.00	1,200	200.0	120.0	1.727	1.040	CONCINICOED	01.72/0	1.10
-																								

DEVELOPMENT	22-28 ANN STREET			
CONSULTANT	WSP Canada Group Limited		DESIGNED BY	IB
MAJOR DRAINAGE AREA		MISSISSAUGA Transportation and Works	CHECKED BY	AK

#### 10 YEAR PRE-DEVELOPMENT STORM HGL ANALYSIS

LOCATION OF SITE	W H From Upstream #	S To Downstream #	(B) US Invert	() DS Invert	W US Obvert	B DS Obvert	Ground Elevation ((	3 Length	900 (%)	B Diameter	<i>⊘</i> Pipe Capacity	© Peak Flow	edols 190 (%)	US HGL	DS HGL	Surcharge Above Obvert @ US MH	Distance Below Surface @ US MH
Park Street E	23	25	77.11	76.50	77.41	76.80	78.79	39.6	1.54	300	120.0	129.3	1.787	83.59	82.89	6.18	-4.80
Park Street E	25	26	76.66	76.51	76.96	76.81	77.88	18.3	0.81	300	87.0	254.6	6.930	82.89	81.62	5.93	-5.01
Park Street E	26	27	76.28	76.04	76.73	76.49	78.09	29.0	0.81	450	256.6	378.2	1.760	81.62	81.11	4.89	-3.53
Park Street E	27	35	76.12	76.05	76.57	76.50	78.88	6.1	1.25	450	318.8	373.9	1.720	81.11	81.00	4.54	-2.23
Elizabeth Street	35	37	76.05	75.72	76.65	76.32	79.53	70.1	0.47	600	420.9	780.6	1.616	81.00	79.87	4.36	-1.48
	37	40	75.72	75.63	76.32	76.23	77.38	18.3	0.47	600	420.9	804.8	1.718	79.87	79.56	3.55	-2.49
Elizabeth Street	40	42	75.72	75.63	76.23	76.23	77.20	33.5	0.47	600	420.9	845.1	1.716	79.56	79.50	3.33	-2.49
Elizabeth Street	40	21	75.63	75.44	76.23	76.07	77.31	7.6	0.47	600	420.9	833.8	1.844	79.50	78.78	2.85	-1.61
Elizabeth Street	42	21	15.41	75.44	70.07	70.04	11.31	7.0	0.44	000	407.3	033.0	1.044	70.92	70.70	2.00	-1.01
High Street E	21	48	75.44	75.20	76.26	76.02	77.69	80.8	0.30	825	786.2	1,963.9	1.872	78.78	77.27	2.52	-1.09
High Street E	48	50	75.19	75.03	76.02	75.86	76.83	53.3	0.30	825	786.2	2,013.0	1.967	77.27	76.22	1.25	-0.44
Ann Street	68	70	81.38	80.77	81.68	81.07	82.93	39.9	1.54	300	120.0	274.9	8.081	88.01	84.78	6.32	-5.08
Ann Street	70	72	80.77	80.70	81.07	81.00	82.24	6.1	1.25	300	108.1	270.7	7.835	84.78	84.30	3.71	-2.54
Aim ou eet			00.77	00.70	01.07	01.00	02.21	0.1	1.20	000	100.1	270.7	7.000	01.70	01.00	0.71	2.01
Park Street E	72	74	80.62	79.86	80.99	80.23	82.48	57.9	1.32	375	201.4	335.4	3.660	84.30	82.18	3.31	-1.82
Park Street E	74	76	79.86	79.48	80.23	79.85	81.26	36.6	1.04	375	178.8	392.8	5.019	82.18	80.35	1.95	-0.92
Park Street E	76	66	79.40	79.10	79.85	79.55	80.83	32.0	0.95	450	277.9	450.5	2.497	80.35	79.55	0.50	0.49
Helene Street N	66	78	77.88	76.81	78.48	77.41	81.38	61.0	1.75	600	812.3	882.7	2.067	78.75	77.49	0.27	2.63
Helene Street N Helene Street N	78	80	76.50	75.59	77.10	76.19	79.02	53.3	1.73	600	805.3	895.8	2.128	77.49	76.35	0.27	1.53
Helene Street N	80	50	75.69	75.59	76.29	76.19	77.14	6.1	1.72	600	805.3	909.8	2.126	76.35	76.22	0.06	0.79
Helene Street N	50	97	74.98	74.95	76.18	76.19	77.14	13.7	0.25	1,200	1,949.4	2,855.9	0.537	76.22	76.15	0.00	1.06
Helene Street N	97	Trunk	74.95	74.65	76.15	75.85	77.15	120.0	0.25	1,200	1,949.4	3,542.3	0.826	76.84	75.85	0.69	0.32

Notes

DEVELOPMENT	22-28 ANN STREET
CONSULTANT	WSP Canada Group Limited

MAJOR DRAINAGE AREA

MISSISSAUGA
Transportation and Works
STORM DRAINAGE DESIGN CHART
FOR CIRCULAR DRAINS FLOWING FULL

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 CHECKED BY
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10 YEAR POST-DEVELOPMENT STORM DESIGN SHEET

March   Marc								10 11	AN FO	OI-DEVEL	.OF WILI	II STORWII	JESIGI	SHLLI												
Property	From	2	Adjacent Contr	ΣΑ		Area Times Run Coefficient	Accumulate Times Rund Coefficient Section	Time of Concentration Opposite an End Section	tc <sub>f</sub>	Time of Concentration at Concentration at Downstream End	intensity of (10 Year Ev	C = Q Quantity of Flow to Pe Accomodated Section	Controlled Flow Section		TOTAL Quantity Flow to be Accomodated in Section		s	☐ Nominal	☐ Nominal	⊢ Length of Se	⊢ Length	Velocity or Pipe Flow	Q	SURCHARGED?	%	
Property													( -7	( -,									,			
Primate   1988			1.35		0.90	1.22																				
Part Service (15)   25   26   15   15   15   15   15   15   15   1					1																					
Mathematic No.   Math			1.68	1.68		1.40	1.40																			
PART No.				-																	_					0.39
Part																										0.25
Taylor   T																										0.30
Second   Control   Contr			5.00			5.00		.5.54	0.00	.0.00	33.02	5.517	3.300	3.000	0.017	3.010	20	. 5.00	.50		3.1	2.004	3.010	JOHO. WINGED		0.00
Part			1.14		0.90	1.03																				
Sign Flower																										
Design   Control   Contr	Upstream	35	1.72	1.72		1.35	1.35																			
Description   Company			0.44		0.90	0.40																				
Exchand Severe (15) 37 64 022 3.84 1.86 1.85 2.26 13.96 0.70 1.67 1.75 1.75 1.75 1.75 1.75 1.75 1.75 1.7																										
Eleaces Served 17(3)			0.66	0.66		0.54	0.54																			
Elasheris Fronce (19) 49 42 022 638																										0.78
File Note   42   21							+														_					0.20
High Riseac Entrols   4.40							+									+										0.38
Park	72		0.00	4.00		0.00	0.20	17.00	0.00	0.34	50.75	0.554	0.000	0.000	0.004	0.010	0.44	24.00	000	20	7.0	1.440	0.407	CONCINENCED	104.7070	0.00
Dept-100			4.40		0.90	3.96																				
High Street E (Tobb)    100   100   080			0.20		0.30	0.06																				
High Street E (1/2)  48 50 0.50 9.56 0.45 7.75 17.44 0.92 18.35 0.60 1.994 0.000 0.000 1.994 0.013 0.30 33.00 825 265 80.8 1.471 0.786 SURCHARGED -145.79% 0.01	Upstream	21	4.60	4.60		4.02	4.02																			
High Street E (1/2)			1.00	1.00	0.90	0.90	0.90																			
High Street E (1/2)   48   50   0.5	21	48			0.50			17.44	0.92	18.35	90.50	1.964	0.000	0.000	1.964	0.013	0.30	33.00	825	265	80.8	1.471	0.786	SURCHARGED	-149.79%	0.92
Park Street E (Total)	48	50	0.50	9.66		0.45	8.20	18.35	0.60	18.96	87.67	2.013	0.000	0.000	2.013	0.013	0.30	33.00	825	175	53.3	1.471	0.786	SURCHARGED	-156.03%	0.60
Park Street E (Total)																										
Ann Street			0.06		0.55	0.03																				
Am Street 70 72 0.00 0.00 0.85 15.39 0.07 15.46 97.65 0.232 0.000 0.000 0.232 0.013 1.25 12.00 300 2.0 6.1 1.530 0.108 SURCHARGED -114.95% 0.0  Park Street E (Total)			0.91		0.90	0.82																				
Park Street E (Total)																										0.39
PROPOSED DEVELOPMENT	70	72	0.00			0.00	0.85	15.39	0.07	15.46	97.65	0.232	0.000	0.000	0.232	0.013	1.25	12.00	300	20	6.1	1.530	0.108	SURCHARGED	-114.95%	0.07
PROPOSED DEVELOPMENT			0.80		0.90	0.72																				
Park Street E (173)						0.72							0.016	0.016												
Park Street E (1/3) 76 66 0.24 1.57 16.36 0.31 16.67 94.10 0.414 0.000 0.016 0.430 0.013 0.95 18.00 450 105 32.0 1.747 0.278 SURCHARGED -54.57% 0.34											_															0.53
Helene St N (Total)				-																						0.38
Helene St N (Total)	76	66				0.24	1.57	10.30	0.31	10.07	94.10	0.414	0.000	0.016	0.430	0.013	0.95	18.00	450	105	32.0	1.747	0.278	SURCHARGED	-54.57%	0.31
Helene St N (1/4) 66 78 0.09 3.25 16.67 0.35 17.02 93.04 0.846 0.000 0.016 0.862 0.013 1.75 24.00 600 200 61.0 2.873 0.812 SURCHARGED -6.15% 0.35 17.02 93.04 0.846 0.000 0.016 0.876 0.013 1.72 24.00 600 200 61.0 2.873 0.812 SURCHARGED -6.15% 0.35 17.02 93.04 0.846 0.000 0.016 0.876 0.013 1.72 24.00 600 175 53.3 2.848 0.805 SURCHARGED -8.74% 0.35 18.00 1.000 0.016 0.800 0.013 1.72 24.00 600 1.75 53.3 2.848 0.805 SURCHARGED -8.74% 0.35 18.00 1.000 0.016 0.800 0.013 1.72 24.00 600 20 6.1 2.848 0.805 SURCHARGED -10.54% 0.05 18.000 0.016 0.800 0.016 0.800 0.013 1.72 24.00 600 20 6.1 2.848 0.805 SURCHARGED -10.54% 0.05 18.000 0.016 0.800 0.	North	66	1.76		0.90	1.58	1.58																			
Helene St N (1/4) 66 78 0.09 3.25 16.67 0.35 17.02 93.04 0.846 0.000 0.016 0.862 0.013 1.75 24.00 600 200 61.0 2.873 0.812 SURCHARGED -6.15% 0.35 17.02 93.04 0.846 0.000 0.016 0.876 0.013 1.72 24.00 600 20 61.0 2.873 0.812 SURCHARGED -6.15% 0.35 17.02 93.04 0.846 0.000 0.016 0.876 0.013 1.72 24.00 600 175 53.3 2.848 0.805 SURCHARGED -8.74% 0.35 17.02 93.04 0.846 0.000 0.016 0.876 0.013 1.72 24.00 600 175 53.3 2.848 0.805 SURCHARGED -8.74% 0.35 17.02 93.04 0.000 0.016 0.876 0.013 1.72 24.00 600 175 53.3 2.848 0.805 SURCHARGED -8.74% 0.35 17.02 93.04 0.000 0.016 0.890 0.013 1.72 24.00 600 20 6.1 2.848 0.805 SURCHARGED -10.54% 0.000 0.016 0.890 0.013 1.72 24.00 600 20 6.1 2.848 0.805 SURCHARGED -10.54% 0.000 0.016 0.890 0.013 0.25 48.00 1.200 45 13.7 1.724 1.949 SURCHARGED -45.59% 0.000 0.016 0			0.42		0.90	0.38																				
Helene St N (1/4) 80 50 0.09 3.44 17.34 0.04 17.37 90.83 0.874 0.000 0.016 0.890 0.013 1.72 24.00 600 20 6.1 2.848 0.805 SURCHARGED -10.54% 0.05																										0.35
Helene St N (1/4) 50 97 0.09 11.73 18.96 0.13 19.09 85.91 2.822 0.000 0.016 2.838 0.013 0.25 48.00 1,200 45 13.7 1.724 1.949 SURCHARGED 45.59% 0.000 0.016 0.000 0.000 0.000 0.000 0.0000 0.00				-												+										0.31
High Street E East 97 2.17 0.90 1.95 2.19				-																						0.04 0.13
High Street E East 97 2.17 0.90 1.95 2.19																										
Helene Street N 97 Trunk 0.81 0.81 0.90 0.73 14.65 19.09 1.16 20.25 85.53 3.509 0.000 0.016 3.525 0.013 0.25 48.00 1,200 230.0 120.0 1.724 1.949 SURCHARGED -80.81% 1.724	East	97	2.17		0.90	1.95	2.19																			
	97	Trunk	0.81	0.81	0.90	0.73	14.65	19.09	1.16	20.25	85.53	3.509	0.000	0.016	3.525	0.013	0.25	48.00	1,200	230.0	120.0	1.724	1.949	SURCHARGED	-80.81%	1.16
		### ### ### ### ### ### ### ### ### ##	### Bank	## ## ## ## ## ## ## ## ## ## ## ## ##	### H## H## A	Bar   Bar	September   Sep	Section   Se	Head   Head			Bar   Bar	Barrier   Barr		## 1	Barrier   Company   Comp				Second Column   Col	March   Marc			Part   Part	Second   Column   C	

DEVELOPMENT	22-28 ANN STREET	

CONSULTANT WSP Canada Group Limited

IAJOR DRAINAGE AREA		

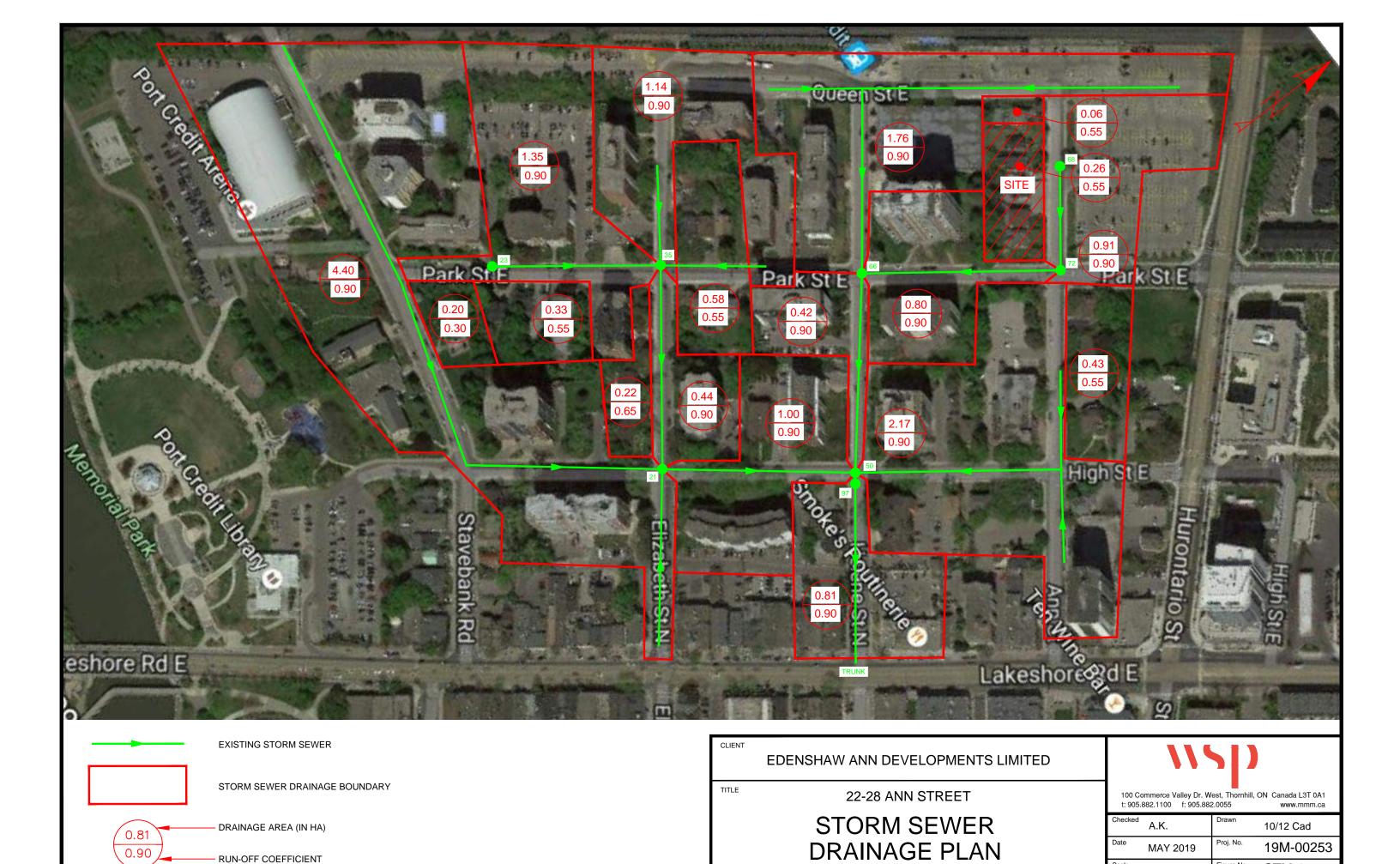
	IMISSISSAUGA Transportation and	
/ Cmm/shmm/	Transportation and	Works

DESIGNED BY	IB	
CHECKED BY	ΔK	

#### 10 YEAR POST-DEVELOPMENT STORM HGL ANALYSIS

LOCATION OF SITE	W H From Upstream	⊠ To Downstream #	() US Invert	B DS Invert	W US Obvert	(B) DS Obvert	Ground Elevation @	3 Length		B Diameter	m3/sm	ু Pipe Capacity	m3/s	ু Peak Flow	(%) HGL Slope	US HGL	DS HGL	Reduction in US HGL  BEVATION as a Result  of Development	Surcharge Above Obvert @ US MH	Distance Below Surface @ US MH
Park Street E	23	25	77.11	76.50	77.41	76.80	78.79	39.6	1.54	300	0.120	120.0	0.129	129.3	1.787	83.59	82.88	0.00	6.18	-4.80
Park Street E	25	26	76.66	76.51	76.96	76.81	77.88	18.3	0.81	300	0.087	87.0	0.255	254.6	6.930	82.88	81.62	0.00	5.93	-5.01
Park Street E	26	27	76.28	76.04	76.73	76.49	78.09	29.0	0.81	450	0.257	256.6	0.378	378.2	1.760	81.62	81.11	0.00	4.89	-3.53
Park Street E	27	35	76.12	76.05	76.57	76.50	78.88	6.1	1.25	450	0.319	318.8	0.374	373.9	1.720	81.11	81.00	0.00	4.53	-2.23
Elizabeth Street	35	37	76.05	75.72	76.65	76.32	79.53	70.1	0.47	600	0.421	420.9	0.781	780.6	1.616	81.00	79.87	0.00	4.36	-1.47
Elizabeth Street	37	40	75.72	75.63	76.32	76.23	77.38	18.3	0.47	600	0.421	420.9	0.805	804.8	1.718	79.87	79.56	0.00	3.55	-2.49
Elizabeth Street	40	42	75.63	75.47	76.23	76.07	77.20	33.5	0.47	600	0.421	420.9	0.845	845.1	1.894	79.56	78.92	0.00	3.33	-2.35
Elizabeth Street	42	21	75.47	75.44	76.07	76.04	77.31	7.6	0.44	600	0.407	407.3	0.834	833.8	1.844	78.92	78.78	0.00	2.85	-1.61
III. b. O F	21	48	75.44	75.20	76.26	76.02	77.69	80.8	0.30	825	0.786	786.2	1.964	1.963.9	1.872	78.78	77.27	0.00	2.52	-1.09
High Street E	48	50	-											,						
High Street E	48	50	75.19	75.03	76.02	75.86	76.83	53.3	0.30	825	0.786	786.2	2.013	2,013.0	1.967	77.27	76.22	0.00	1.25	-0.43
Ann Street	68	70	81.38	80.77	81.68	81.07	82.93	39.9	1.54	300	0.120	120.0	0.236	236.0	5.957	86.49	84.11	1.51	4.81	-3.56
Ann Street	70	72	80.77	80.70	81.07	81.00	82.24	6.1	1.25	300	0.108	108.1	0.232	232.4	5.776	84.11	83.76	0.67	3.04	-1.87
Park Street E	72	74	80.62	79.86	80.99	80.23	82.48	57.9	1.32	375	0.201	201.4	0.313	313.1	3.190	83.76	81.91	0.54	2.77	-1.28
Park Street E	74	76	79.86	79.48	80.23	79.85	81.26	36.6	1.04	375	0.179	178.8	0.371	371.3	4.485	81.91	80.27	0.27	1.68	-0.65
Park Street E	76	66	79.40	79.10	79.85	79.55	80.83	32.0	0.95	450	0.278	277.9	0.430	429.5	2.270	80.27	79.55	0.07	0.42	0.56
Helene Street N	66	78	77.88	76.81	78.48	77.41	81.38	61.0	1.75	600	0.812	812.3	0.862	862.2	1.972	78.63	77.43	0.12	0.16	2.75
Helene Street N	78	80	76.50	75.59	77.10	76.19	79.02	53.3	1.72	600	0.805	805.3	0.876	875.7	2.034	77.43	76.35	0.06	0.33	1.59
Helene Street N	80	50	75.69	75.59	76.29	76.19	77.14	6.1	1.72	600	0.805	805.3	0.890	890.1	2.102	76.35	76.22	0.01	0.05	0.80
Helene Street N	50	97	74.98	74.95	76.18	76.15	77.28	13.7	0.25	1,200	1.949	1,949.4	2.838	2,838.1	0.530	76.22	76.15	0.00	0.04	1.06
Helene Street N	97	Trunk	74.95	74.65	76.15	75.85	77.15	120.0	0.25	1,200	1.949	1,949.4	3.525	3,524.7	0.817	76.83	75.85	0.01	0.68	0.33

Notes



STM-1

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